

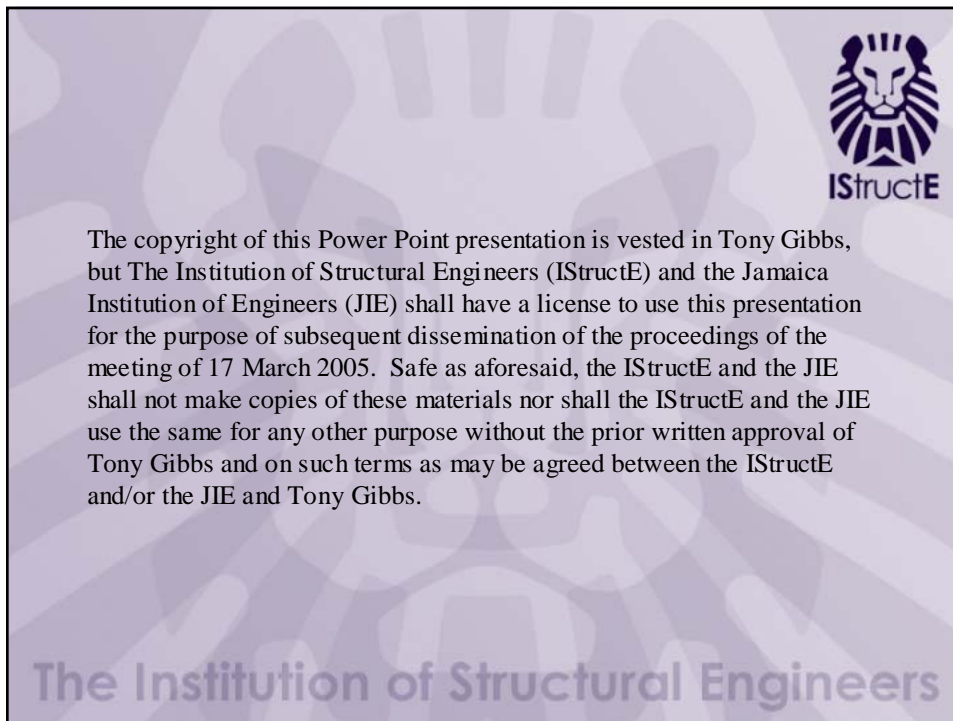


**Code Developments
for
Wind-resistant Design
of
Buildings**



Tony Gibbs


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**History of
Caribbean Wind-loading Standards**



Pre-1950s

CP3 : Chapter V : Part 2 - 1952

South Florida Building Code

Ronan Point - 1968


CCEO-BAPE Standard – 1970

OAS-NCST-CCEO-BAPE Standard – 1981 (BNS CP28)

CUBiC : Part 2 : Section 2


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**A Brief Overview
of Some Important
Wind-loading Standards**



- *ISO 4354 and CUBiC:Part-2:Section-2*
- *ENV 1991-2-4*
- *ASCE 7-98 and DRBC-03*
- *AIJ Recommendations*
- *AS1170.2*
- *Barbados Standard BNS CP28*


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Different International Wind Standards

<i>Standard</i>	<i>Identification</i>
ISO	International Standard Organization
CUBiC	Caribbean Uniform Building Code
ENV	Eurocode
DRBC	Dominican Republic Building Code
AIJ	Japan Standard
AS	Australian Standard
BNSCP	Barbados Standard


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Standard	Averaging Time	Return Period(s)
ISO 4354	10 minutes	50 years
CUBiC	10 minutes	50 years
ENV 1991-2-4	10 minutes	50 years
ASCE 7-98	3 seconds	50 years
AIJ	10 minutes	100 years
AS1170.2-1989	3 seconds	20 and 1000 years
BNS CP28	3 seconds	50 years

Note: Canadian and British standards now use 1-hour averaging time.

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Comparative table with different ways of reporting wind velocity

Averaging time	Wind Velocity (mph)			
1 Hour	120	113	91	79
10 minutes	127	120	96	84
Fastest mile	158	149	120	105
3 second gust	181	171	137	120

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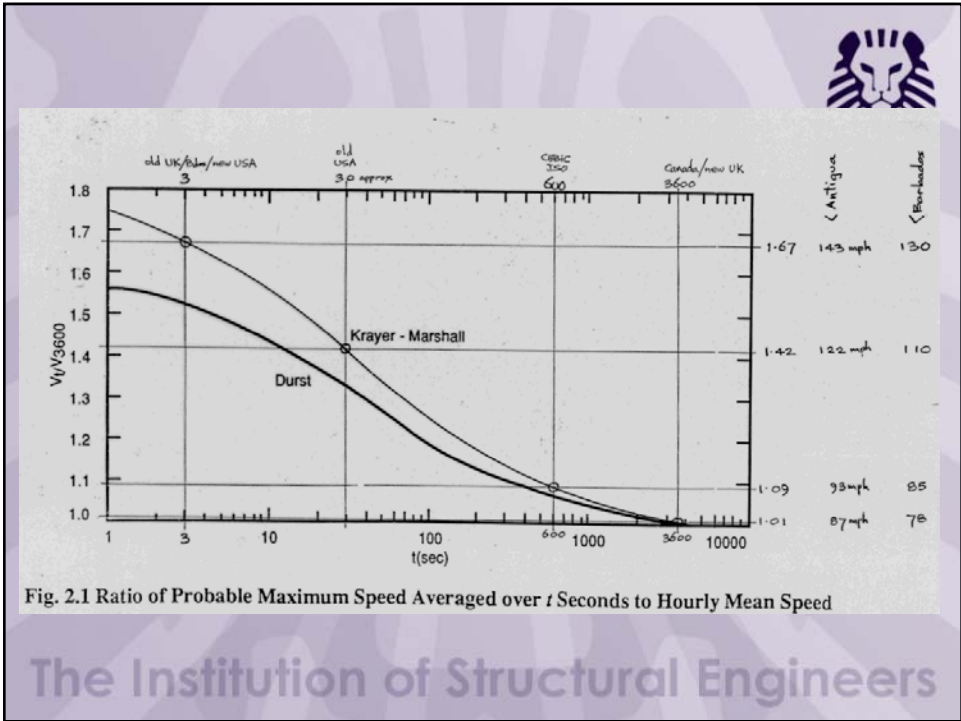




Fig. 2.1 Ratio of Probable Maximum Speed Averaged over t Seconds to Hourly Mean Speed

Differences and similarities for calculating design wind speeds and dynamic pressures


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<i>Standard</i>	<i>Speed</i>	<i>Pressure</i>	<i>Building Pressure/Force</i>
ISO 4354	v	$q_{ref} = \frac{1}{2} \rho V^2$	$W = (q_{ref})(C_{exp})(C_{fig})(C_{dyn})$
CUBIC	v	$q_{ref} = \frac{1}{2} \rho V^2$	$W = q_{ref}(C_{exp})(C_{fig})(C_{dyn})$
ENV 1991-2-4	$V_{ref} = C_{dir}C_{tem}C_{alt}C_{ref,0}$	$q_{ref} = \frac{1}{2} \rho (V_{ref})^2$	$W_e = q_{ref}C_{exp}(Z_e)C_{pe}$
DRBC-03	$V(3s - gust)$	$q_z = \frac{1}{2} \rho K_z K_{zt} K_d IV^2$	$p = q_z(GC_p) - q_h(GC_{pi})$
AIJ	$U_H = U_g E_f E_g R$	$q_h = \frac{1}{2} \rho U_H^2$	$W_f = q_h C_f G_f A$
AS1170.2-89	$V_z = V_{z,cat} M_s M_t M_i$	$q_h = \frac{1}{2} \rho V_z^2$	$P_e = C_{p,e} K_a K_1 K_p q_z$
BNSCP28	v	$q = \frac{1}{2} \rho (VS_1 S_2 S_3)^2$	$P = q C_{pe}$

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Building Shape or Type	ISO 4354	CUBiC	ENV 1991	ASCE 7-98	AIJ	AS1170 .2	BNS CP28
stepped roofs	no	no	no	yes	no	no	yes
free-standing walls	yes	yes	yes	yes	no	yes	no
free-standing roofs	no	no	yes	no	no	yes	yes
attached canopies	no	no	no	no	no	yes	yes
multispan roofs	no	no	yes	yes	yes	yes	yes
multispan canopies	no	no	yes	no	no	no	no
arched roofs	yes	yes	yes	yes	yes	yes	yes
domes	no	no	yes	no	yes	no	no
bins, silos, tanks	yes	yes	yes	no	no	yes	no
circular sections	yes	yes	yes	yes	yes	yes	yes
polygonal sections	no	no	yes	no	no	yes	yes
structural angle	yes	yes	yes	no	no	yes	yes
bridge decks	no	yes	yes	no	no	no	no
lattice sections	yes	yes	yes	yes	no	yes	yes
flags	no	no	yes	no	no	no	no
spheres	no	yes	yes	no	no	no	yes

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**The trend for Caribbean standards
is to adopt and adapt
the ASCE-7 approach**
(Dominican Republic, new CUBiC, Cayman, Bahamas)


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ASCE 7 Methods

- Method 1: Simplified (tables & limited use)
- **Method 2: Analytical (almost all cases)**
- Method 3: Wind Tunnel (unusual cases)

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Method 1: Simplified

The building must be:

1. a simple diaphragm building;
2. a low-rise building;
3. **enclosed and conform to the wind-borne debris provisions;**
4. **a regular shaped building or structure;**
5. not classified as a flexible building;
6. **not assessed as having unfavourable aerodynamic characteristics and not having an unfavourable site location;**
7. of a structure with no expansion joints or separations;
8. **not subject to unfavourable topographic effects;**
9. **of an approximately symmetrical cross section.**

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Summary for Method 2

- MWFRS
 - $p = q GC_p - q_i (GC_{pi})$
- C&C for $h \leq 60$ ft
 - $p = q_h [(GC_p) - (GC_{pi})]$
- where:
 - $q_z = 0.00256 K_z K_{zt} K_d V^2 I$
 - $q_h = 0.00256 K_h K_{zt} K_d V^2 I$

p = design pressure
 q = effective velocity pressure
 G = gust effect factor (gef)
 C_p = external pressure coefficient
 q_i = velocity pressure (internal)
 GC_{pi} = gef + internal pressure coefficient
 GC_p = gef + external pressure coefficient
 K_z = exposure velocity pressure coefficient
 K_{zt} = topographic factor
 K_d = directionality factor
 V = basic wind speed
 I = importance factor

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The first step in Method 2 is to determine the appropriate parameters for evaluating the velocity pressure, q



Parameter	Symbol	What does it mean?
Directionality	K_d	Takes into account the probability that the maximum wind has the same direction than that of the maximum pressure
Importance	I	Converts a 50-year return period into a 100-year return period recommended for hospitals
Exposure	K_z	Represents the wind velocity at height z above the ground in different terrains
Topography	K_{zt}	Takes into account the fact that the structure be located on top of a hill or on a escarpment increasing the wind velocity


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Meaning of factors in ASCE-7



Name	Symbol	What does it mean?
Gust Factor	G	Represents the turbulence-structure interaction and the corresponding dynamic amplification
External Pressure Coefficient	C_p	Represents the wind pressure on the building's external walls
Internal Pressure Coefficient	C_{pi}	Reflects the internal pressure due to quantity and sizes of wall openings
Design Pressure	p	Represents the design pressure
Design Force	F	Represents the net force on open structures

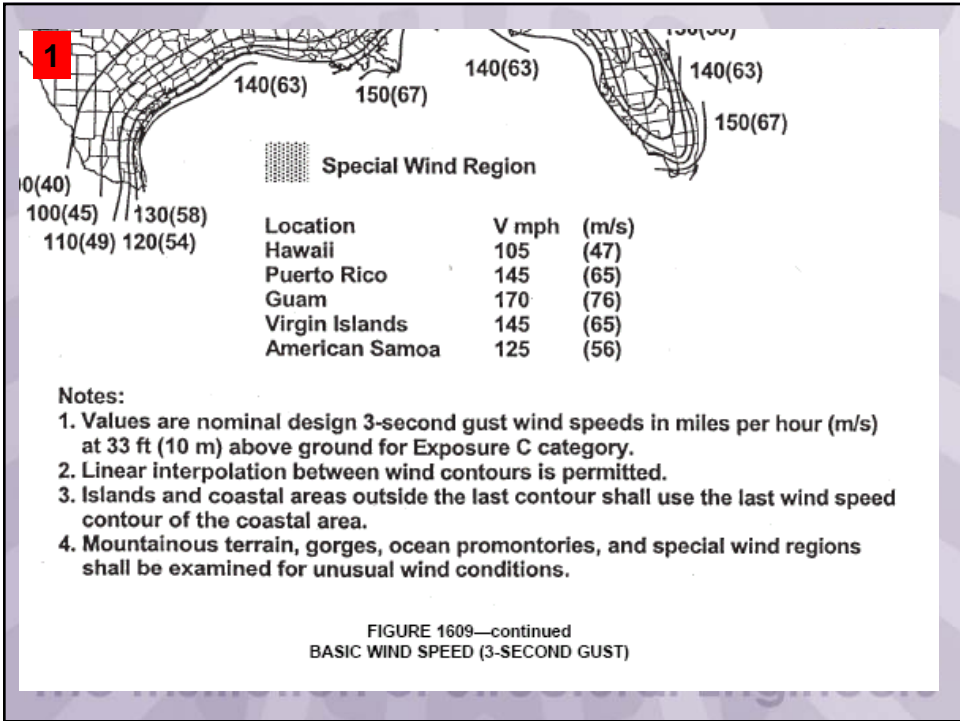
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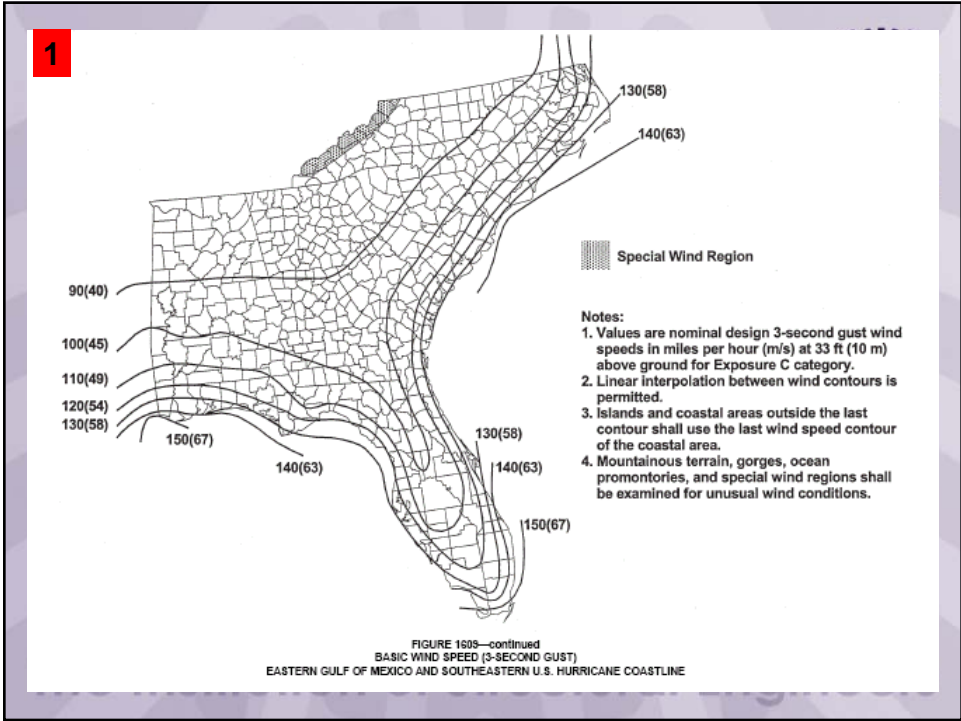


Method 2: Analytical

1. basic wind speed V and wind directionality factor K_d
2. importance factor I
3. exposure category or exposure categories and velocity pressure exposure coefficient K_z or K_h
4. topographic factor K_{zt}
5. gust effect factor G or G_f
6. enclosure classification
7. internal pressure coefficient GC_{pi}
8. external pressure coefficients C_p or GC_{pf} or force coefficient C_f
9. velocity pressure q_z or q_h
10. design wind load p or F


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1

Directionality Factor K_d



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Structure Type	K_d
Buildings	
Main Wind Force Resisting System	0.85
Components and Cladding	0.85
Arched Roofs	0.85
Chimneys, Tanks, and Similar Structures	
Square	0.90
Hexagonal	0.95
Round	0.95
Open Signs and Lattice Framework	0.85
Trussed Towers	
Triangular, square, rectangular	0.85
All other cross sections	0.95

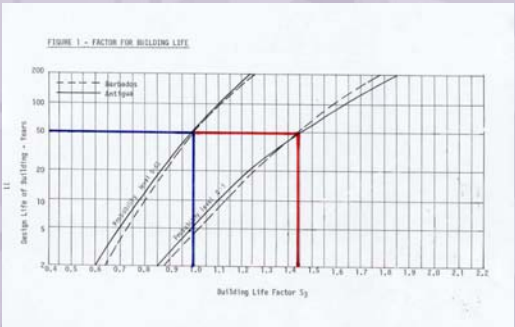
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2

Importance Factor *I*




$$I = \left(\frac{V_{100}}{V_{50}} \right)^2 \text{ or } \left(\frac{V_{25}}{V_{50}} \right)^2$$



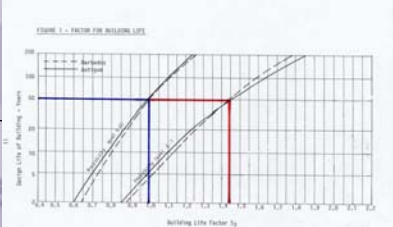
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2

Importance Factor *I*




Category	Non-Hurricane Prone Regions, Hurricane Prone Regions with V=85-100 mph, and Alaska	Hurricane Prone Regions with V>100 mph
I	0.87	0.77
II	1.00	1.00
III	1.15	1.15
IV		1.15



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3


Velocity Pressure Exposure Coefficient K_z


$$V_z = V_{33} \left(\frac{z}{33} \right)^{1/\alpha}$$

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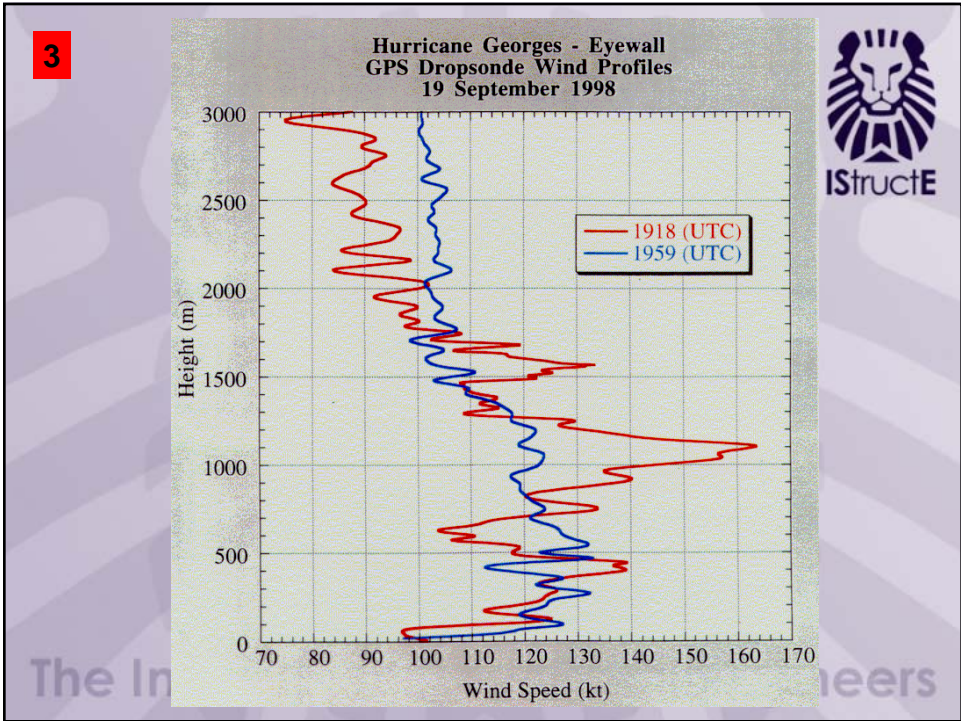
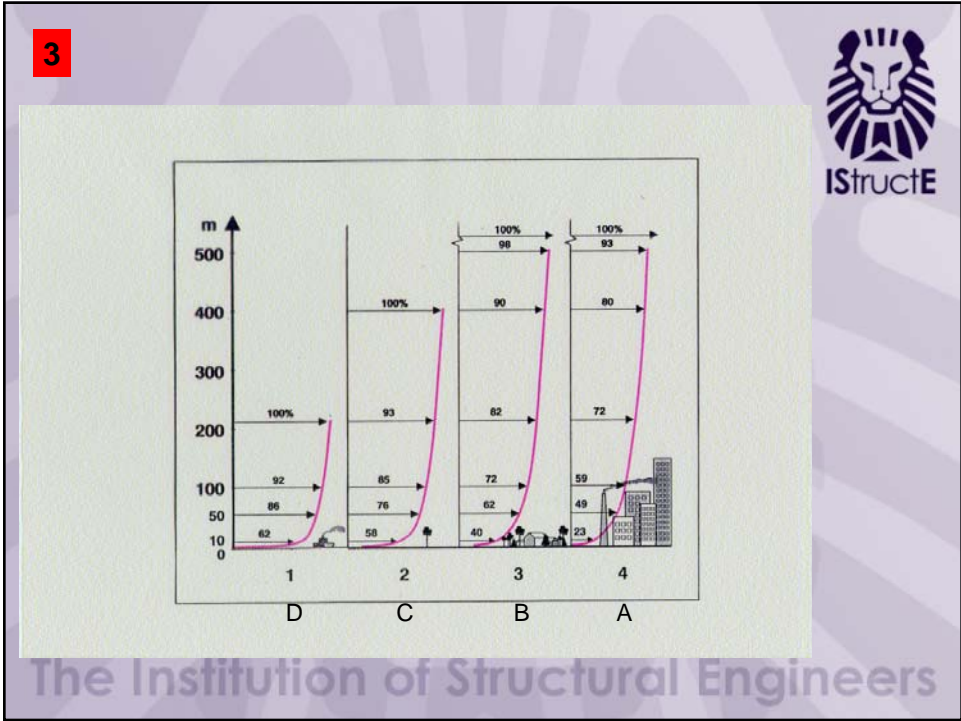
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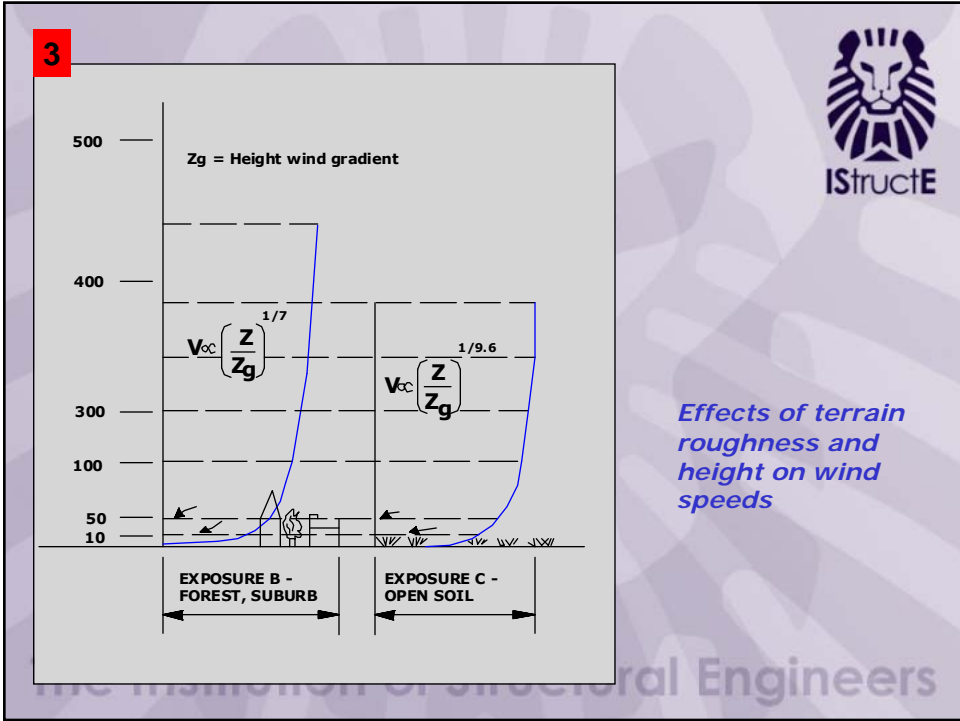
Exposure Constants



Exposure Category	Gradient Height	$1/\alpha$
A	1500 ft	1/5
B	1200 ft	1/7
C	900 ft	1/9.5
D	700 ft	1/11.5

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3

K_z

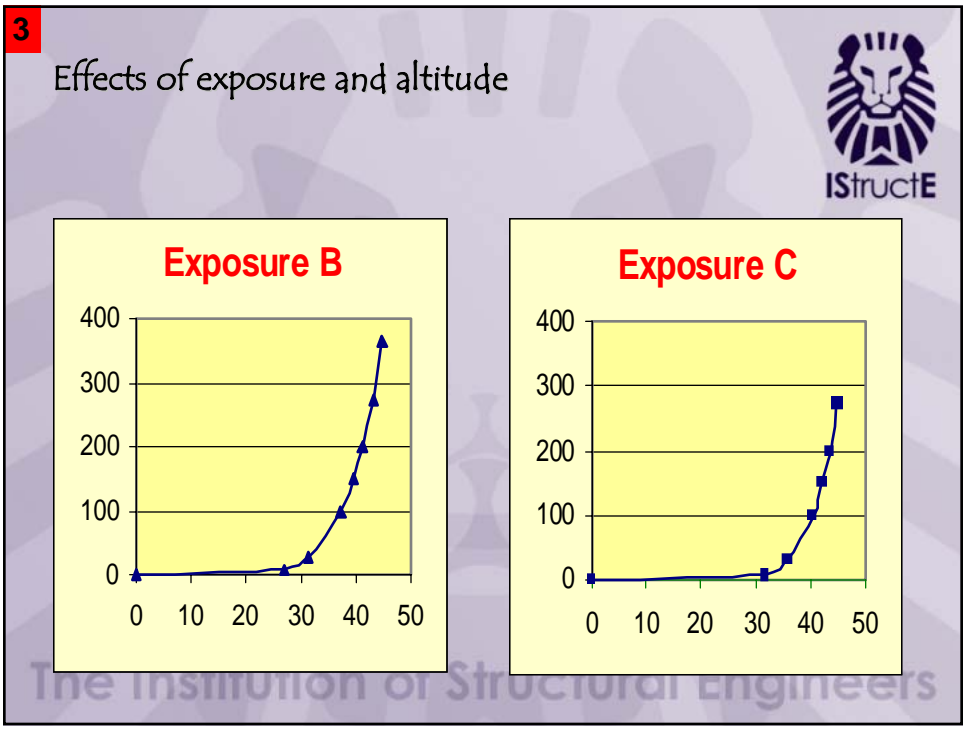
$$V_g = \left[V_{33} \left(\frac{900}{33} \right)^{1/9.5} \right]$$

$$V_z = V_g \left(\frac{z}{z_g} \right)^{\alpha} = \left[1.42 V_{33} \right] \left(\frac{z}{z_g} \right)^{\alpha}$$

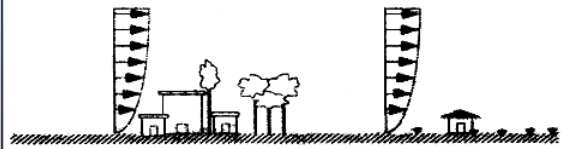
$$K_z = \left(\frac{V_z}{V_{33}} \right)^2 = 2.01 \left(\frac{z}{z_g} \right)^{2\alpha}$$

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3 Exposure Coefficients K_z, K_h



Exposure type **B**
C

Height Z (m)	Exposure B			Exposure C		
	Case 1	Case 2	Case 1 y 2	Case 1	Case 2	Case 1 y 2
≤ 5	.70	.57	.85	32	1.03	1.30
6	.70	.62	.90	34	1.07	1.34
8	.70	.67	.96	36	1.10	1.37
10	.72	.72	1.00	38	1.14	1.4
12	.76	.76	1.04	40	1.17	1.43
14	.79	.79	1.07	42	1.20	1.46
16	.82	.82	1.11	44	1.23	1.48
18	.85	.85	1.13	46	1.25	1.51
20	.88	.88	1.16	48	1.28	1.53
22	.90	.90	1.18	50	1.30	1.55
24	.92	.92	1.20	52	1.32	1.57
26	.93	.93	1.21	54	1.35	1.59
28	.96	.96	1.24	56	1.37	1.61
30	.98	.98	1.26	58	1.39	1.63

NOTE:

1. **Case 1** shall be used for all primary systems in buildings with height 'h' less than 18 m and for secondary systems of any type of structure
2. **Case 2** shall be used for all primary systems of any other structure not indicated in case 1
3. For values of **Z** not shown, linear interpolation shall be permitted

3

K_z and K_h

Velocity Pressure Coefficients, K_h and K_z



Height above ground level, z ft (m)	A	B	C	D
0-15 (0-4.6)	0.32	0.57	0.85	1.03
20 (6.1)	0.36	0.62	0.90	1.08
25 (7.6)	0.39	0.66	0.94	1.12
30 (9.1)	0.42	0.70	0.98	1.16
40 (12.2)	0.47	0.76	1.04	1.22
50 (15.2)	0.52	0.81	1.09	1.27
60 (18)	0.55	0.85	1.13	1.31
70 (21.3)	0.59	0.89	1.17	1.34
80 (24.4)	0.62	0.93	1.21	1.38
90 (27.4)	0.65	0.96	1.24	1.40
100 (30.5)	0.68	0.99	1.26	1.43

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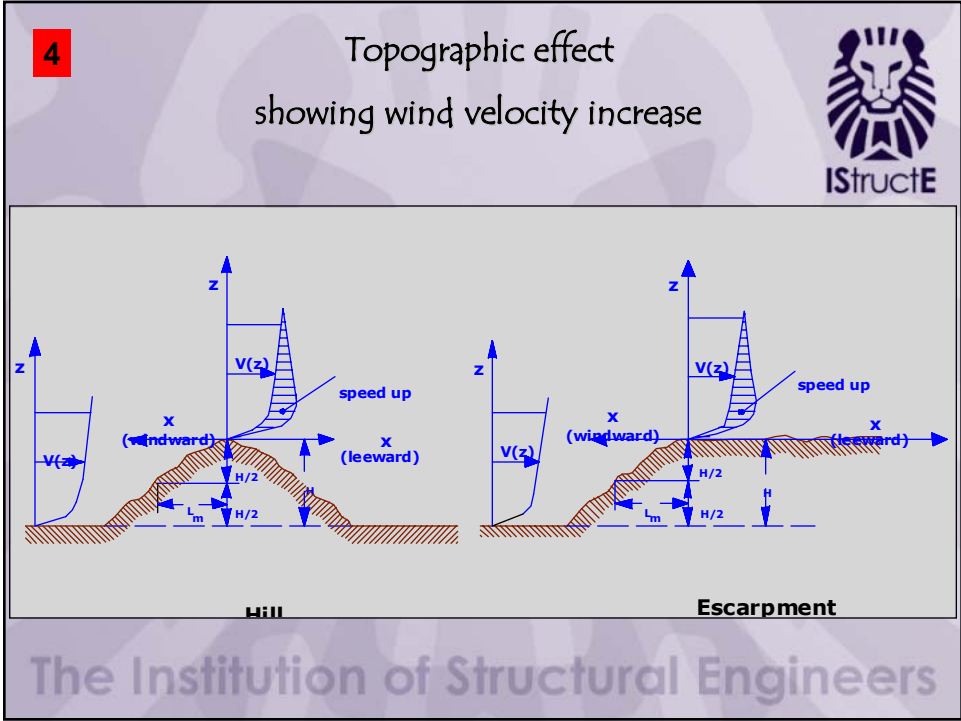
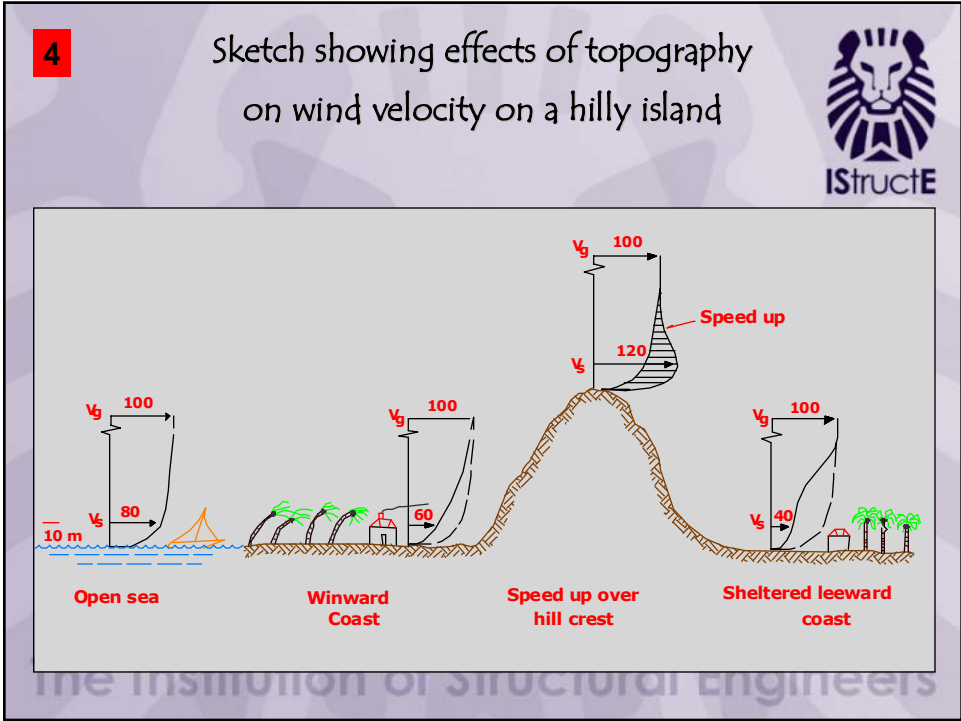
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Topographic Factor K_{zt}

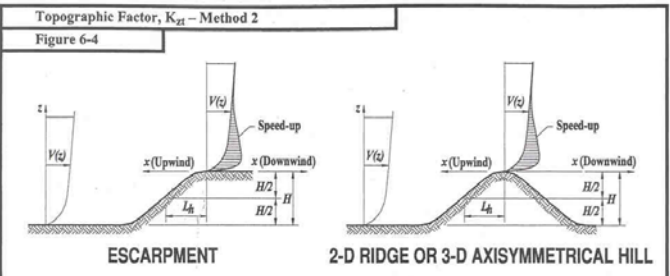


$$K_{zt} = [1 + K_1 K_2 K_3]^2$$

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4



Topographic Multipliers for Exposure C

H/L _h	K ₁ Multiplier			x/L _h	K ₂ Multiplier		z/L _h	K ₃ Multiplier		
	2-D Ridge	2-D Escarp.	3-D Axisym. Hill		2-D Escarp.	All Other Cases		2-D Ridge	2-D Escarp.	3-D Axisym. Hill
0.20	0.29	0.17	0.21	0.00	1.00	1.00	0.00	1.00	1.00	1.00
0.25	0.36	0.21	0.26	0.50	0.88	0.67	0.10	0.74	0.78	0.67
0.30	0.43	0.26	0.32	1.00	0.75	0.33	0.20	0.55	0.61	0.45
0.35	0.51	0.30	0.37	1.50	0.63	0.00	0.30	0.41	0.47	0.30
0.40	0.58	0.34	0.42	2.00	0.50	0.00	0.40	0.30	0.37	0.20
0.45	0.65	0.38	0.47	2.50	0.38	0.00	0.50	0.22	0.29	0.14
0.50	0.72	0.43	0.53	3.00	0.25	0.00	0.60	0.17	0.22	0.09
				3.50	0.13	0.00	0.70	0.12	0.17	0.06
				4.00	0.00	0.00	0.80	0.09	0.14	0.04
							0.90	0.07	0.11	0.03
							1.00	0.05	0.08	0.02
							1.50	0.01	0.02	0.00
							2.00	0.00	0.00	0.00

$$K_{zt} = [1 + K_1 K_2 K_3]^2$$



5

Gust Effect Factor G or G_f

- Gust intensity
- Gust frequency
- Gust size
 - Integral scale longitudinal and lateral
- Frequency of structure
- Structural damping
- Aerodynamic admittance
- Gust correlation




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Gust Effect Factor G

Rigid Structures: Complete Analysis



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$$G = 0.925 \left[\frac{1 + 1.7 g_Q I_z Q}{1 + 1.7 g_v I_z} \right]$$

g_Q = peak factor for background response
 I_z = intensity of turbulence
 Q = background response factor
 g_v = peak factor for wind response

$$Q^2 = \frac{1}{1 + 0.63 \left(\frac{B+h}{L_z} \right)^{0.63}}$$


L_z = integral length scale of turbulence

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Gust Effect Factor G_f

MWFRS for flexible buildings and other structures



IStructE

$$G_f = 0.925 \left[\frac{1 + 1.7 I_z \sqrt{g_Q^2 Q^2 g_R^2 R^2}}{1 + 1.7 g_v I_z} \right]$$

g_Q = peak factor for background response
 g_R = peak factor for resonant response
 R = resonant response factor
 I_z = intensity of turbulence
 Q = background response factor
 g_v = peak factor for wind response

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Building, Enclosed

A building that does not comply with the requirements for open or partially enclosed buildings.

Building, Open

A building having each wall at least 80%.

This condition is expressed for each wall by the equation:

$$A_o \geq 0.8 A_g, \text{ where}$$

A_o = total area of openings in a wall that receives positive external pressure, in ft²

A_g = the gross area of that wall in which A_o is identified, in ft²

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Building, Partially Enclosed



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1. The total area of openings in a wall that receives positive external pressure exceeds the sum of the areas of openings in the balance of the building envelope (walls and roof) by more than 10%, and
2. The total area of openings in a wall that receives positive external pressure exceeds 0.37 m² (4 ft²) or 1% of the area of that wall, whichever is smaller, and the percentage of openings in the balance of the building envelope does not exceed 20%.

1. $A_o > 1.10 A_{oi}$

2. $A_o > 4 \text{ ft}^2$ or $> 0.01 A_g$, whichever is smaller,
and $A_{oi}/A_{gi} \leq 0.20$

where

A_o, A_g are as defined for Open Building

A_{oi} = the sum of the areas of openings in the


building envelope (walls and roof) not including

A_o , in ft²

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GC_{pi} Gust Factor combined with Internal Pressure Coefficient




Enclosure Classification	GC_{pi}
Open Buildings	0.00
Partially Enclosed Buildings	+0.55 -0.55
Enclosed Buildings	+0.18 -0.18

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Analytical Method for MWFRS



$$q_z = 0.00256 K_z K_{zt} K_d V^2 I$$

$$p = qGC_p - q_i(GC_{pi})$$

for all rigid buildings

$$p = q_h[(GC_{pf}) - (GC_{pi})]$$


alternate for low-rise rigid buildings

$$p = qG_f C_p - q_i(GC_{pi})$$

for flexible buildings

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8



Design pressure on primary systems (structural)

Rigid Primary Systems


$$p = q GC_p - q_i (GC_{pi})$$


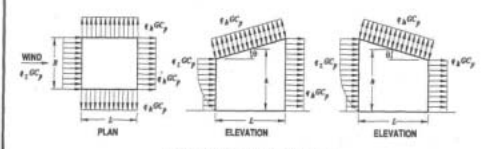
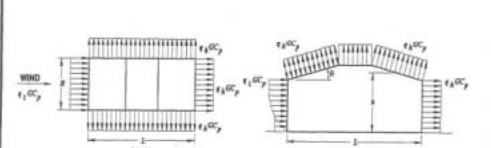
Flexible Primary Systems

$$p = qG_f C_p - q_i (GC_{pi})$$

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8



Main Wind Force Resisting System - Method 2	All Heights
Figure 6-6 External Pressure Coefficients, C_p	Walls & Roofs
Enclosed, Partially Enclosed Buildings	
 <p style="text-align: center;">GABLE, HIP ROOF</p>	 <p style="text-align: center;">MONOSLOPE ROOF (NOTE 4)</p>
 <p style="text-align: center;">MANSARD ROOF (NOTE 8)</p>	

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Main Wind Force Resisting System - Method 2		All Heights											
Figure 6-4 (cont'd) External Pressure Coefficients, C_p		Walls & Roofs											
Enclosed, Partially Enclosed Buildings													
Wall Pressure Coefficients, C_p													
Surface	L/B	C_p	Use With										
Windward Wall	All values	0.8	q_s										
		0-1	-0.5										
Leeward Wall	2	-0.3	q_s										
	20	-0.2											
Side Wall	All values	-0.7	q_s										
Roof Pressure Coefficients, C_p , for use with q_s													
Wind Direction	Windward												
	Angle, θ (degrees)												
	h/L	10	15	20	25	30	35	45	$\geq 60^\circ$	10	15	≥ 20	
Normal to ridge for $\theta \geq 10^\circ$	≤ 0.25	-0.7	-0.5	-0.3	-0.2	-0.2	0.0*	0.4	0.4	0.01 θ	-0.3	-0.3	-0.6
	≥ 0.5	-0.9	-0.7	-0.4	-0.3	-0.2	-0.2	0.0*	0.4	0.01 θ	-0.5	-0.5	-0.6
Normal to ridge for $0 < \theta < 10^\circ$	≤ 0.5	-1.3**	-1.0	-0.7	-0.5	-0.3	-0.2	0.0*	0.4	0.01 θ	-0.7	-0.6	-0.6
	≥ 1.0	-0.18	-0.18	-0.18	0.0*	0.2	0.2	0.2	0.3	0.01 θ	-0.7	-0.6	-0.6
Parallel to ridge for all θ	≤ 0.5	Horiz distance from windward edge		C_p		*Value is provided for interpolation purposes.							
		0 to h/2	-0.6		-0.18		**Value can be reduced linearly with area over which it is applicable as follows						
		h/2 to h	-0.5		-0.18								
Area (sq ft)	Reduction Factor												
	≤ 100 (9.3 sq m)	1.0											
≥ 200 (18.3 sq m)	0.9												
≥ 1000 (92.9 sq m)	0.8												

Notes:

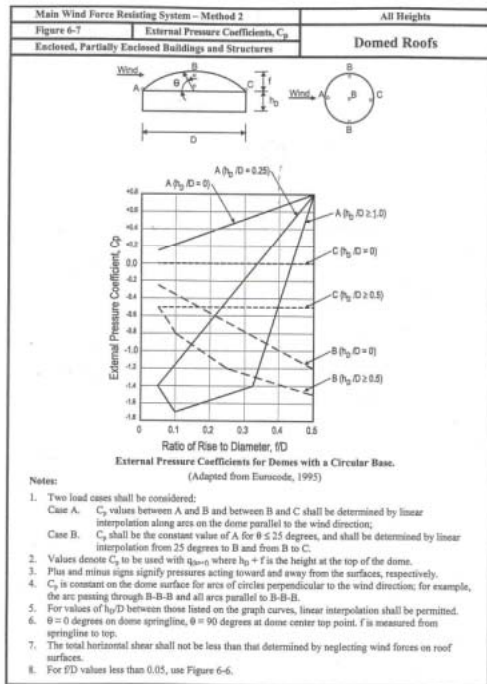
- Plus and minus signs signify pressures acting toward and away from the surfaces, respectively.
- Linear interpolation is permitted for values of L/B, h/L and θ other than shown. Interpolation shall only be carried out between values of the same sign. Where no value of the same sign is given, assume 0.0 for interpolation purposes.
- Where two values of C_p are listed, this indicates that the windward roof slope is subjected to either positive or negative pressures and the roof structure shall be designed for both conditions. Interpolation for intermediate ratios of h/L, in this case shall only be carried out between C_p values of like sign.
- For monoslope roofs, entire roof surface is either a windward or leeward surface.
- For flexible buildings use appropriate G as determined by Section 6.2.4.
- Refer to Figure 6-7 for domes and Figure 6-8 for arched roofs.
- Notation:
 - B: Horizontal dimension of building, in feet (meter), measured normal to wind direction.
 - L: Horizontal dimension of building, in feet (meter), measured parallel to wind direction.
 - h: Mean roof height in feet (meters), except that eave height shall be used for $\theta \leq 10$ degrees.
 - x: Height above ground, in feet (meters).
 - G: Gust effect factor.
 - q_s : Velocity pressure, in pounds per square foot (N/m^2), evaluated at respective height.
 - θ : Angle of plane of roof from horizontal, in degrees.
- For mansard roofs, the top horizontal surface and leeward inclined surface shall be treated as leeward surfaces from the table.
- Except for MWFRS's at the roof consisting of moment resisting frames, the total horizontal shear shall not be less than that determined by neglecting wind forces on roof surfaces.
- For roof slopes greater than 80° , use $C_p = 0.8$.



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Main Wind Force Res. Sys. / Comp and Clad. – Method 2		All Heights		
Figure 6-8 External Pressure Coefficients, C_p		Arched Roofs		
Enclosed, Partially Enclosed Buildings and Structures				
Conditions	Rise-to-span ratio, r	C_p		
		Windward quarter	Center half	Leeward quarter
Roof on elevated structure	$0 < r < 0.2$	-0.9	$-0.7 - r$	-0.5
	$0.2 \leq r < 0.3^*$	$1.5r - 0.3$	$-0.7 - r$	-0.5
	$0.3 \leq r \leq 0.6$	$2.75r - 0.7$	$-0.7 - r$	-0.5
Roof springing from ground level	$0 < r \leq 0.6$	$1.4r$	$-0.7 - r$	-0.5

*When the rise-to-span ratio is $0.2 \leq r \leq 0.3$, alternate coefficients given by 6r - 2.1 shall also be used for the windward quarter.

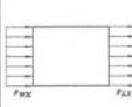
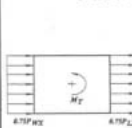
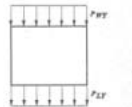
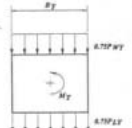
Notes:

1. Values listed are for the determination of average loads on main wind force resisting systems.
2. Plus and minus signs signify pressures acting toward and away from the surfaces, respectively.
3. For wind directed parallel to the axis of the arch, use pressure coefficients from Fig. 6-6 with wind directed parallel to ridge.
4. For components and cladding: (1) At roof perimeter, use the external pressure coefficients in Fig. 6-1 with θ based on spring-line slope and (2) for remaining roof areas, use external pressure coefficients of this table multiplied by 0.87.

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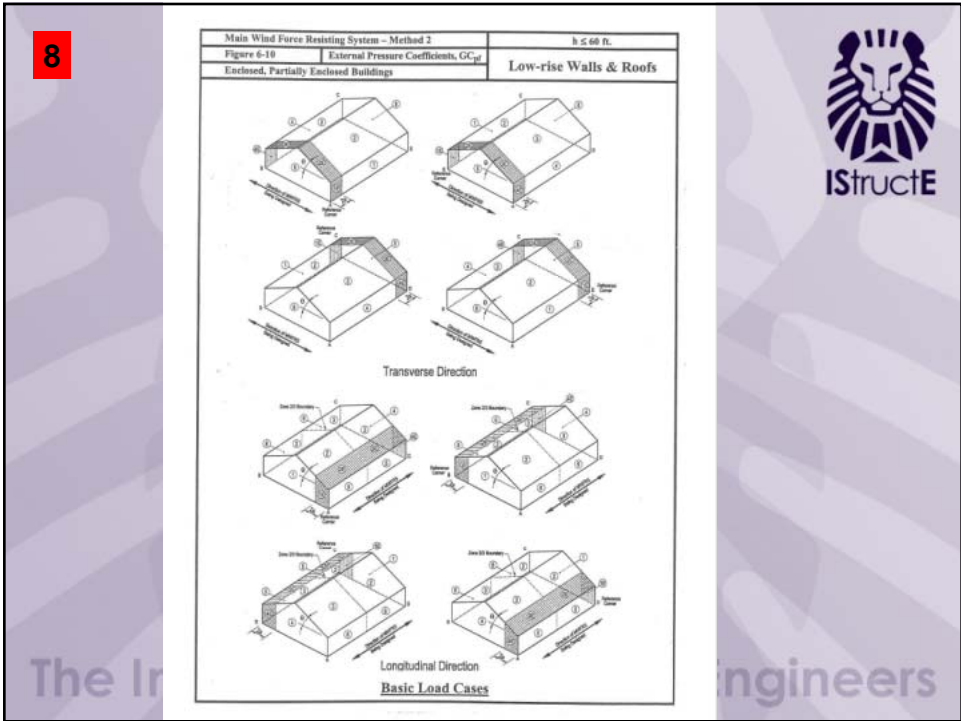
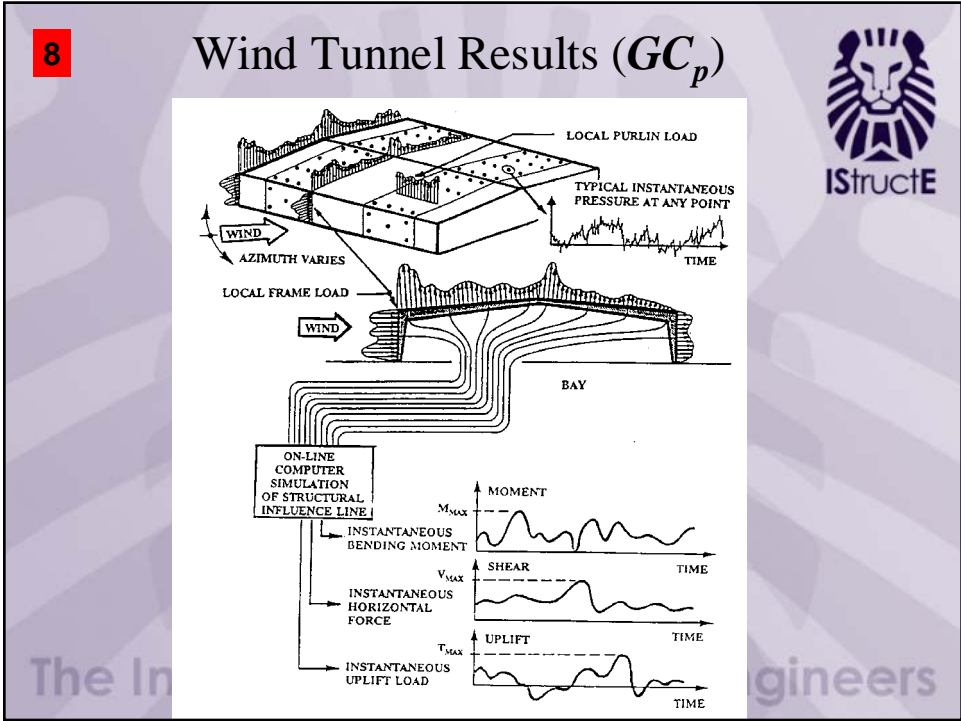
Main Wind Force Resisting System— Method 2		All Heights		
Figure 6-9 Design Wind Load Cases		Arched Roofs		
 <p>CASE 1</p>	 <p>CASE 2</p>	 <p>CASE 3</p>	 <p>CASE 4</p>	
$M_T = 0.75 (P_{wy} - P_{lx}) B_T e_T$ $e_T = \pm 0.15 B_T$		$M_T = 0.75 (P_{wy} - P_{lx}) B_T e_T$ $e_T = \pm 0.15 B_T$		$M_T = 0.563 (P_{wy} - P_{lx}) B_T e_T + 0.563 (P_{wy} - P_{lx}) B_T e_T$ $e_T = \pm 0.15 B_T$

Notes:

- Case 1. Full design wind pressure acting on the projected area perpendicular to each principal axis of the structure, considered separately along each principal axis.
- Case 2. Three quarters of the design wind pressure acting on the projected area perpendicular to each principal axis of the structure in conjunction with a torsional moment as shown, considered separately for each principal axis.
- Case 3. Wind loading as defined in Case 1, but considered to act simultaneously at 75% of the specified value.
- Case 4. Wind loading as defined in Case 2, but considered to act simultaneously at 75% of the specified value.

Notes:

1. Design wind pressures for windward and leeward faces shall be determined in accordance with the provisions of 6.5.12.2.1 and 6.5.12.2.3 as applicable for building of all heights.
2. Diagrams show plan views of building.
3. Notation:
 P_{wx}, P_{wy} : Windward face design pressure acting in the x, y principal axis, respectively.
 P_{lx}, P_{ly} : Leeward face design pressure acting in the x, y principal axis, respectively.
 e_T : Eccentricity for the x, y principal axis of the structure, respectively.
 M_T : Torsional moment per unit height acting about a vertical axis of the building.



8

Main Wind Force Resisting System - Method 2		h ≤ 60 ft.								
Figure 6-10 (cont'd) External Pressure Coefficients, C _{pe}		Low-rise Walls & Roofs								
Enclosed, Partially Enclosed Buildings										
Roof Angle θ (degrees)	Building Surface									
	1	2	3	4	5	6	1E	2E	3E	4E
0-5	0.40	-0.69	-0.37	-0.29	-0.45	-0.45	0.61	-1.07	-0.53	-0.43
10	0.53	-0.69	-0.48	-0.43	-0.45	-0.45	0.80	-1.07	-0.69	-0.64
30-45	0.56	0.21	-0.43	-0.37	-0.45	-0.45	0.69	0.27	-0.53	-0.48
90	0.56	0.56	-0.37	-0.37	-0.45	-0.45	0.69	0.69	-0.48	-0.48

Notes:

1. Plus and minus signs signify pressures acting toward and away from the surfaces, respectively.
2. For values of θ other than those shown, linear interpolation is permitted.
3. The building must be designed for all wind directions using the 8 loading patterns shown. The load patterns are applied to each building corner in turn as the Reference Corner.
4. Combinations of external and internal pressures (see Figure 6-5) shall be evaluated as required to obtain the most severe loadings.
5. For the torsional load cases shown below, the pressures in zones designated with a "T" (1T, 2T, 3T, 4T) shall be 25% of the full design wind pressures (zones 1, 2, 3, 4).
Exception: One story buildings with h less than or equal to 30 ft (9.1m), buildings two stories or less framed with light frame construction, and buildings two stories or less designed with flexible diaphragms need not be designed for the torsional load cases.
Torsional loading shall apply to all eight basic load patterns using the figures below applied at each reference corner.
6. Except for moment-resisting frames, the total horizontal shear shall not be less than that determined by neglecting wind forces on roof surfaces.
7. For the design of the MWFRS providing lateral resistance in a direction parallel to a ridge line or for flat roofs, use θ = 0° and locate the zone 2/3 boundary at the mid-length of the building.
8. The roof pressure coefficient C_{pe}, when negative in Zone 2, shall be applied in Zone 2 for a distance from the edge of roof equal to 0.5 times the horizontal dimension of the building parallel to the direction of the MWFRS being designed or 2.5h, whichever is less; the remainder of Zone 2 extending shall use the pressure coefficient C_{pe} for Zone 3.
9. Notation:
a: 10 percent of least horizontal dimension or 0.4h, whichever is smaller, but not less than either 4% of least horizontal dimension or 3 ft (0.9 m).
h: Mean roof height, in feet (meters), except that eave height shall be used for θ ≤ 10°.
θ: Angle of plane of roof from horizontal, in degrees.

Torsional Load Cases



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Analytical Method for Components & Cladding



$$q_z = 0.00256 K_z K_{zt} K_d V^2 I$$

$$p = q_h[(GC_p) - (GC_{pi})]$$

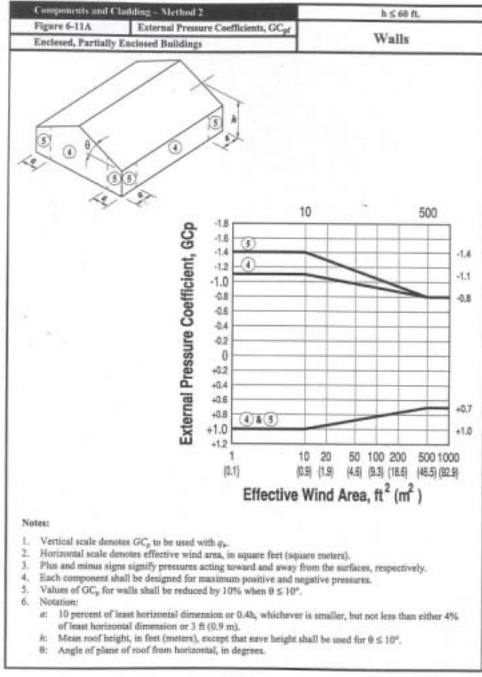
for buildings with $h \leq 60$ ft

$$p = q(GC_p) - q_i(GC_{pi})$$

for buildings with $h > 60$ ft

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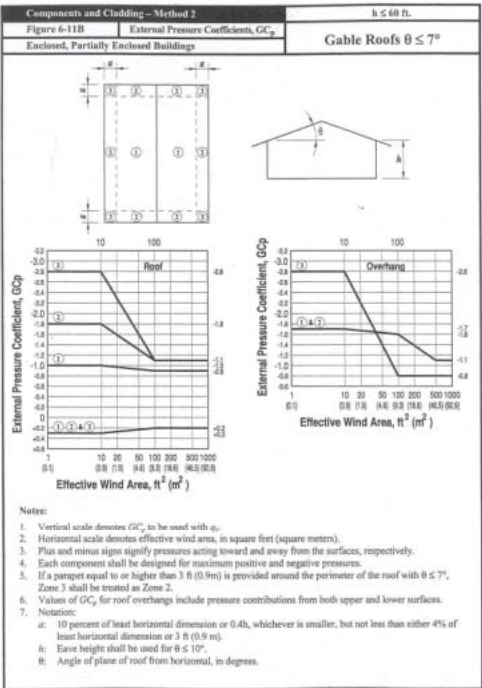
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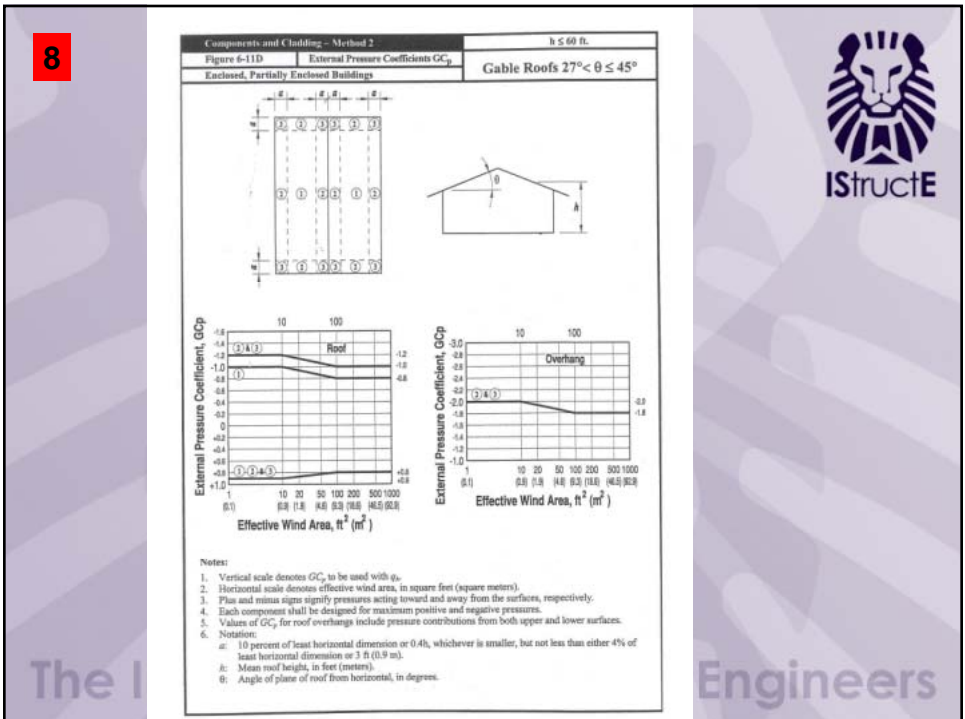
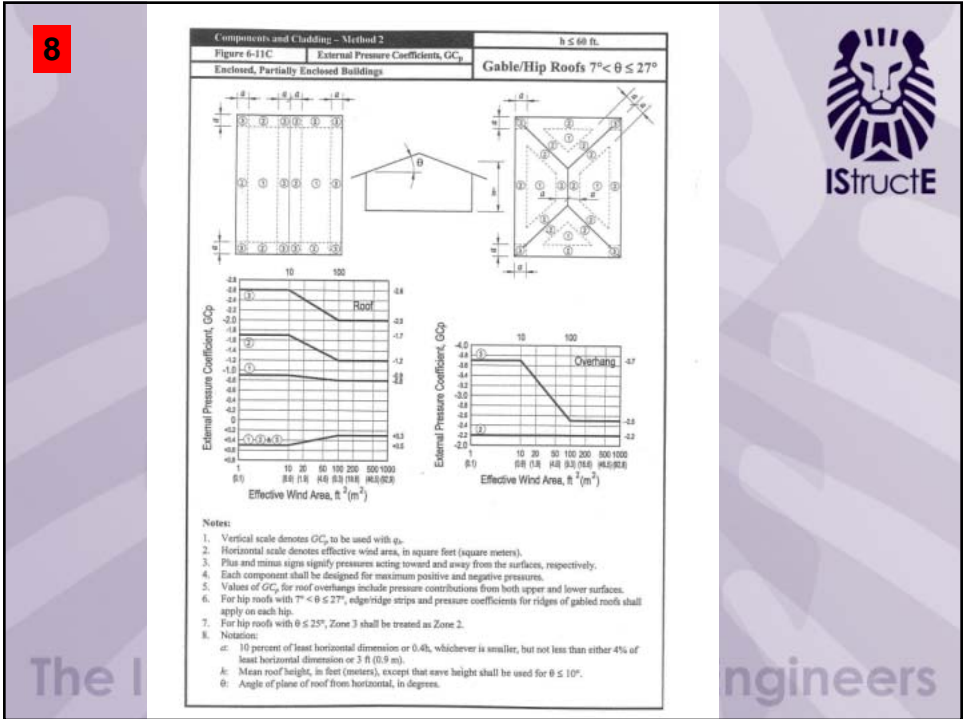
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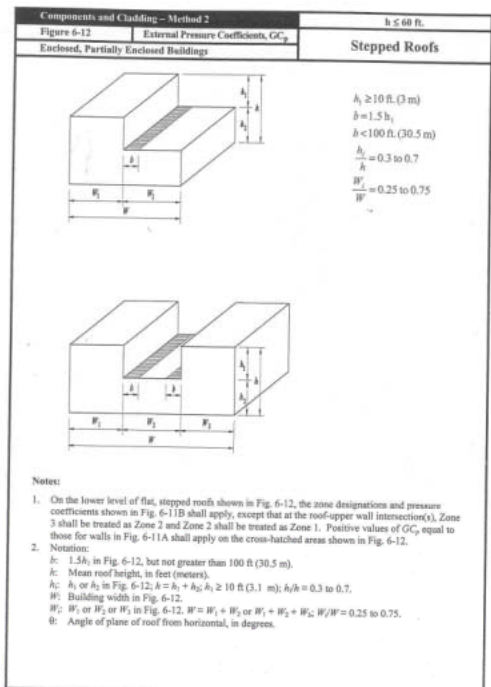


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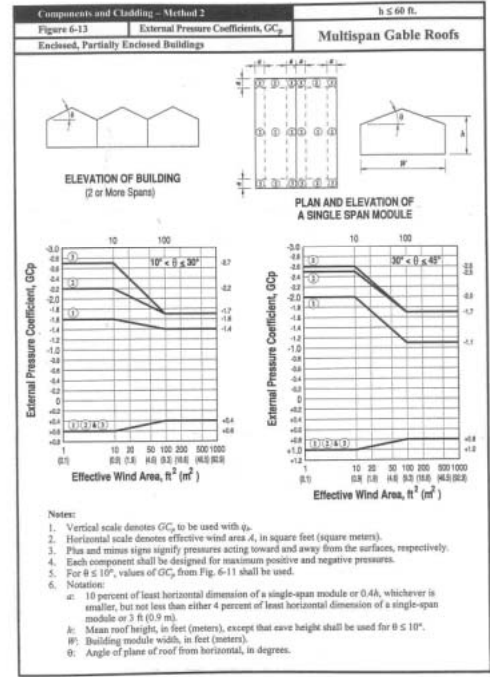
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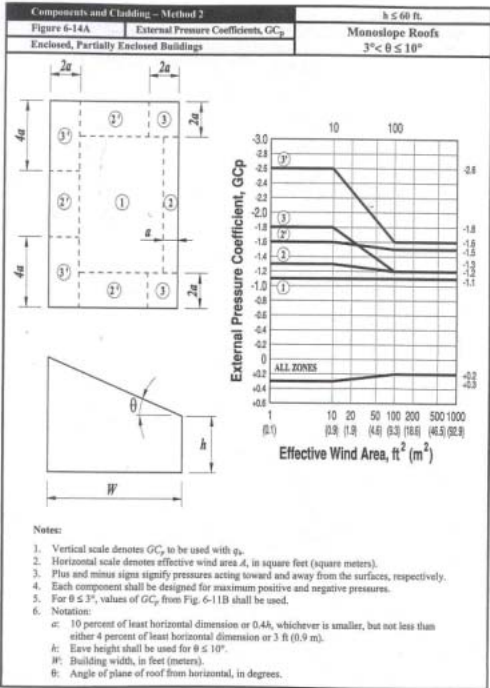
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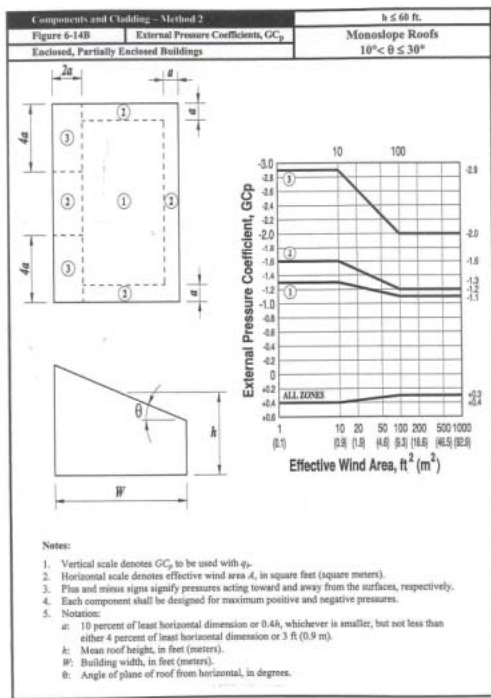
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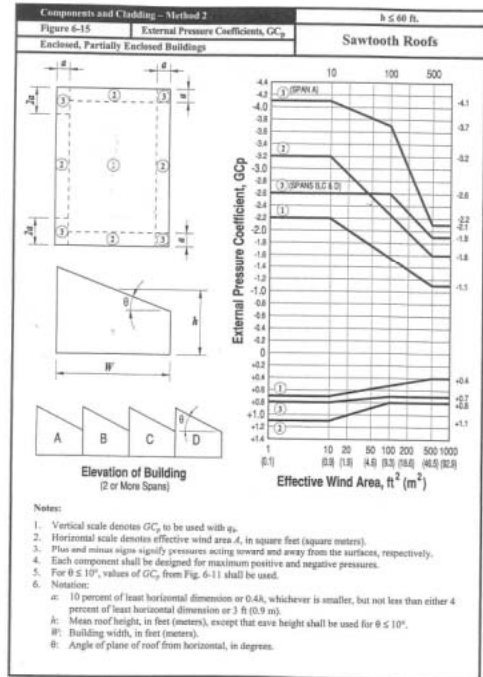
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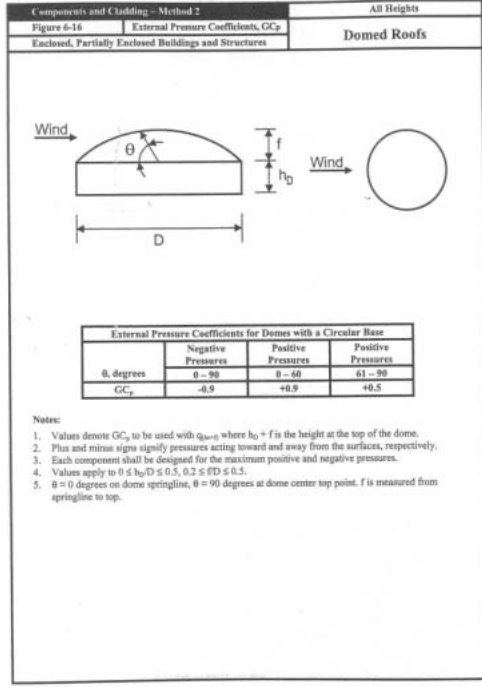
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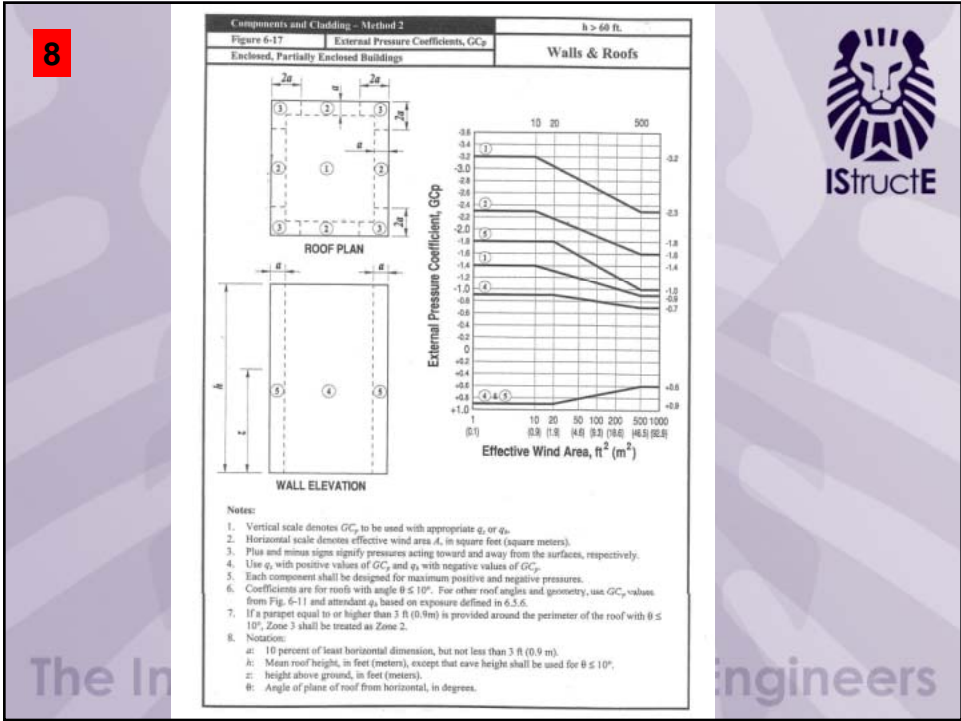
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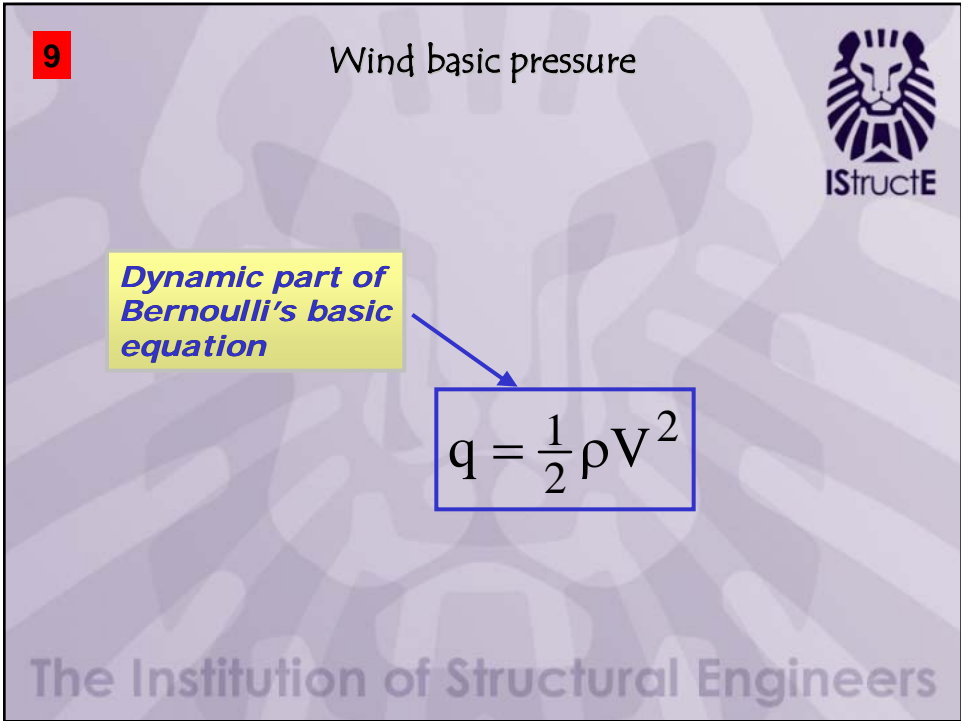


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Constant 0.00256



$$P = \frac{1}{2} \rho V^2$$

$$P = \frac{1}{2} \left(\frac{0.0765}{32.2} \right) \left(\frac{5280}{3600} \right)^2 V^2$$

$$P = 0.00256 V^2$$

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Modified basic pressure in ASCE-7
to accommodate local parameters



**modified basic pressure:
ASCE-7**

$$q = \frac{1}{2} \rho K_z K_{zt} K_d IV^2$$

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9

Velocity Pressure



$$q_z = 0.00256 K_z K_{zt} K_d V^2 I$$

$$q_h = 0.00256 K_h K_{zt} K_d V^2 I$$

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9 & 10

Analytical Method for Open Buildings and Other Structures




$$q_z = 0.00256 K_z K_{zt} K_d V^2 I$$

$$F = q_z G C_f A_f$$

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10

Design pressure for components and cladding
and design force for special and open structures



Design pressure

$$p = q_h [(GC_p) - (GC_{pi})]$$

Design force

$$F = q_z GC_f A_f$$


towers, signs, tanks, silos

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8

Main Wind Force Resisting System – Method 2
Figure 6-18 Force Coefficients, C_f

Open Buildings



All Heights
Monoslope Roofs

Roof angle θ degrees	L/B						
	s	3	2	1	3/2	1/3	1/8
10	0.2	0.25	0.3	0.45	0.55	0.7	0.75
15	0.35	0.45	0.5	0.7	0.85	0.9	0.85
20	0.5	0.6	0.75	0.9	1.0	0.95	0.9
25	0.7	0.8	0.95	1.15	1.1	1.05	0.95
30	0.9	1.0	1.2	1.3	1.2	1.1	1.0

Roof angle θ degrees	Center of Pressure X/L		
	L/B		
	2 to 5	1	1/5 to 1/2
10 to 20	0.35	0.3	0.3
25	0.35	0.35	0.4
30	0.35	0.4	0.45

Notes:

1. Wind forces act normal to the surface. Two cases shall be considered: (1) wind forces directed inward; and (2) wind forces directed outward.
2. The roof angle shall be assumed to vary a 10° from the actual angle and the angle resulting in the greatest force coefficient shall be used.
3. Notation:
 - B: dimension of roof measured normal to wind direction, in feet (meters);
 - L: Dimension of roof measured parallel to wind direction, in feet (meters);
 - X: Distance to center of pressure from windward edge of roof, in feet (meters); and
 - θ : Angle of plane of roof from horizontal, in degrees.


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Other Structures - Method 2		All Heights		
Figure 6-19	Force Coefficients, C_f	Chimneys, Tanks, Rooftop Equipment, & Similar Structures		
Cross-Section	Type of Surface	h/D		
		1	7	28
Square (wind normal to face)	All	1.3	1.4	2.0
Square (wind along diagonal)	All	1.0	1.1	1.5
Hexagonal or octagonal	All	1.0	1.2	1.4
Round ($D\sqrt{q_z} > 2.5$) ($D\sqrt{q_z} > 5.3$, D in m, q_z in N/m^2)	Moderately smooth	0.5	0.6	0.7
	Rough ($D/D = 0.02$)	0.7	0.8	0.9
	Very rough ($D/D = 0.08$)	0.8	1.0	1.2
Round ($D\sqrt{q_z} \leq 2.5$) ($D\sqrt{q_z} \leq 5.3$, D in m, q_z in N/m^2)	All	0.7	0.8	1.2

Notes:

- The design wind force shall be calculated based on the area of the structure projected on a plane normal to the wind direction. The force shall be assumed to act parallel to the wind direction.
- Linear interpolation is permitted for h/D values other than shown.
- Notation:
 - D: diameter of circular cross-section and least horizontal dimension of square, hexagonal or octagonal cross-sections at elevation under consideration, in feet (meters);
 - D': depth of protruding elements such as ribs and spoilers, in feet (meters); and
 - h: height of structure, in feet (meters); and
 - q_z : velocity pressure evaluated at height z above ground, in pounds per square foot (N/m^2).




8

Other Structures - Method 2		All Heights	
Figure 6-20	Force Coefficients, C_f	Solid Freestanding Walls & Solid Signs	
At Ground Level		Above Ground Level	
v	C_f	M/N	C_f
≤3	1.2	≤6	1.2
5	1.3	10	1.3
8	1.4	16	1.4
10	1.5	20	1.5
20	1.75	40	1.75
30	1.85	60	1.85
≥40	2.0	≥80	2.0

Notes:

- The term "signs" in notes below applies also to "freestanding walls".
- Signs with openings comprising less than 30% of the gross area shall be considered as solid signs.
- Signs for which the distance from the ground to the bottom edge is less than 0.25 times the vertical dimension shall be considered to be at ground level.
- To allow for both normal and oblique wind directions, two cases shall be considered:
 - a. resultant force acts normal to the face of the sign on a vertical line passing through the geometric center; and
 - b. resultant force acts normal to the face of the sign at a distance from a vertical line passing through the geometric center equal to 0.2 times the average width of the sign.
- Notation:
 - v: ratio of height to width;
 - M: larger dimension of sign, in feet (meters); and
 - N: smaller dimension of sign, in feet (meters).




8

Other Structures – Method 2		All Heights	
Figure 6-21	Force Coefficients, C_f	Open Signs & Lattice Frameworks	
e	Flat-Sided Members	Rounded Members	
		$D\sqrt{q_z} \leq 2.5$ ($D\sqrt{q_z} \leq 5.3$)	$D\sqrt{q_z} > 2.5$ ($D\sqrt{q_z} > 5.3$)
< 0.1	2.0	1.2	0.8
0.1 to 0.29	1.8	1.3	0.9
0.3 to 0.7	1.6	1.5	1.1

Notes:

- Signs with openings comprising 30% or more of the gross area are classified as open signs.
- The calculation of the design wind forces shall be based on the area of all exposed members and elements projected on a plane normal to the wind direction. Forces shall be assumed to act parallel to the wind direction.
- The area A_f consistent with these force coefficients is the solid area projected normal to the wind direction.
- Notation:
 e : ratio of solid area to gross area;
 D : diameter of a typical round member, in feet (meters);
 q_z : velocity pressure evaluated at height z above ground in pounds per square foot (N/m^2).



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Other Structures – Method 2		All Heights	
Figure 6-22	Force Coefficients, C_f	Trussed Towers	
Open Structures			
Tower Cross Section	C_f		
Square	$4.0 e^2 - 5.9 e + 4.0$		
Triangle	$3.4 e^2 - 4.7 e + 3.4$		

Notes:

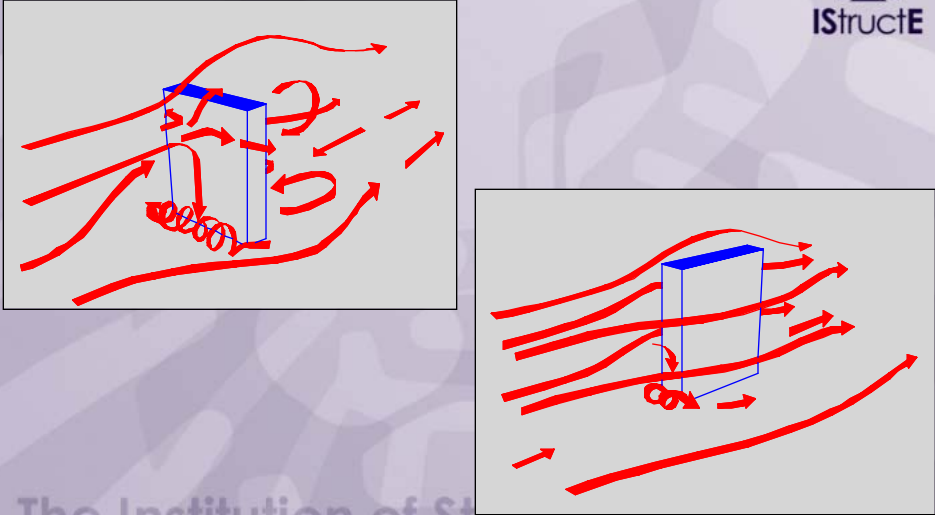
- For all wind directions considered, the area A_f consistent with the specified force coefficients shall be the solid area of a tower face projected on the plane of that face for the tower segment under consideration.
- The specified force coefficients are for towers with structural angles or similar flat-sided members.
- For towers containing rounded members, it is acceptable to multiply the specified force coefficients by the following factor when determining wind forces on such members:
 $0.51 e^2 + 0.57$, but not > 1.0
- Wind forces shall be applied in the directions resulting in maximum member forces and reactions. For towers with square cross-sections, wind forces shall be multiplied by the following factor when the wind is directed along a tower diagonal:
 $1 + 0.75 e$, but not > 1.2
- Wind forces on tower appurtenances such as ladders, conduits, lights, elevators, etc., shall be calculated using appropriate force coefficients for these elements.
- Loads due to ice accretion as described in Section 11 shall be accounted for.
- Notation:
 e : ratio of solid area to gross area of one tower face for the segment under consideration.




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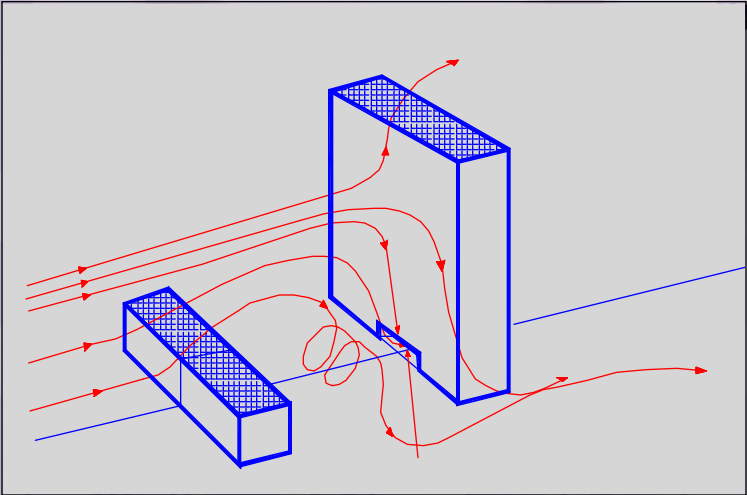
Turbulent flow of wind on longitudinal and transverse sides of high rise buildings




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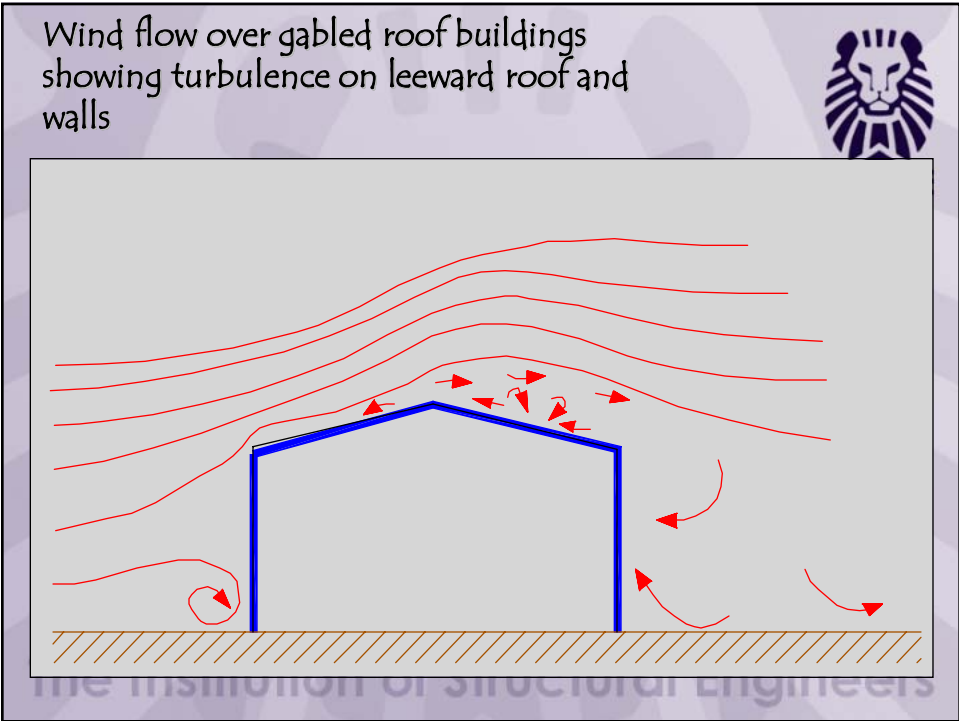
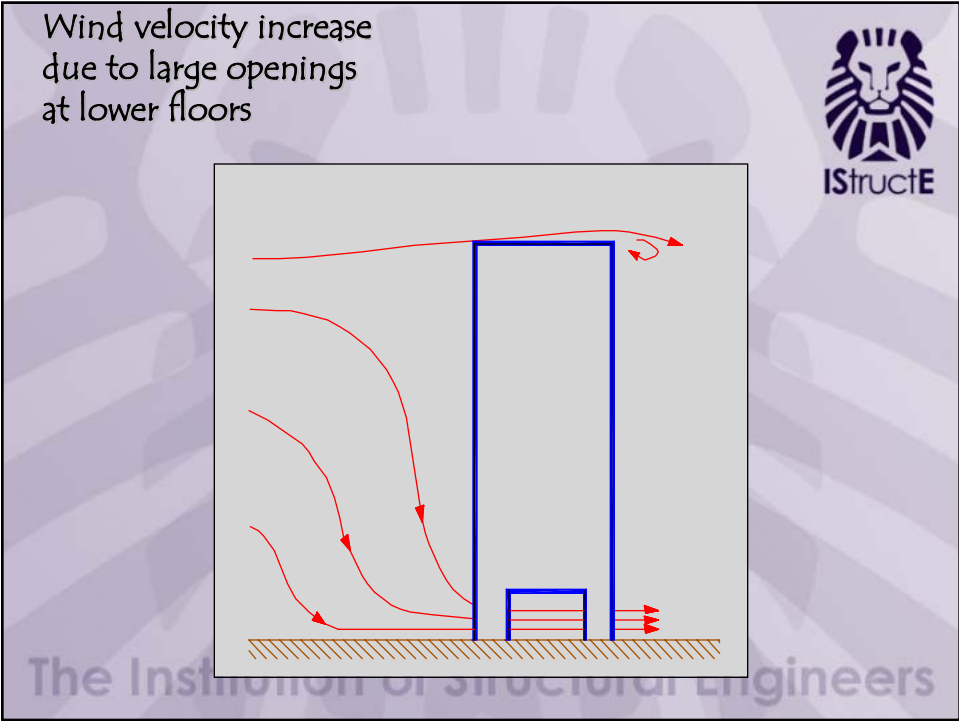


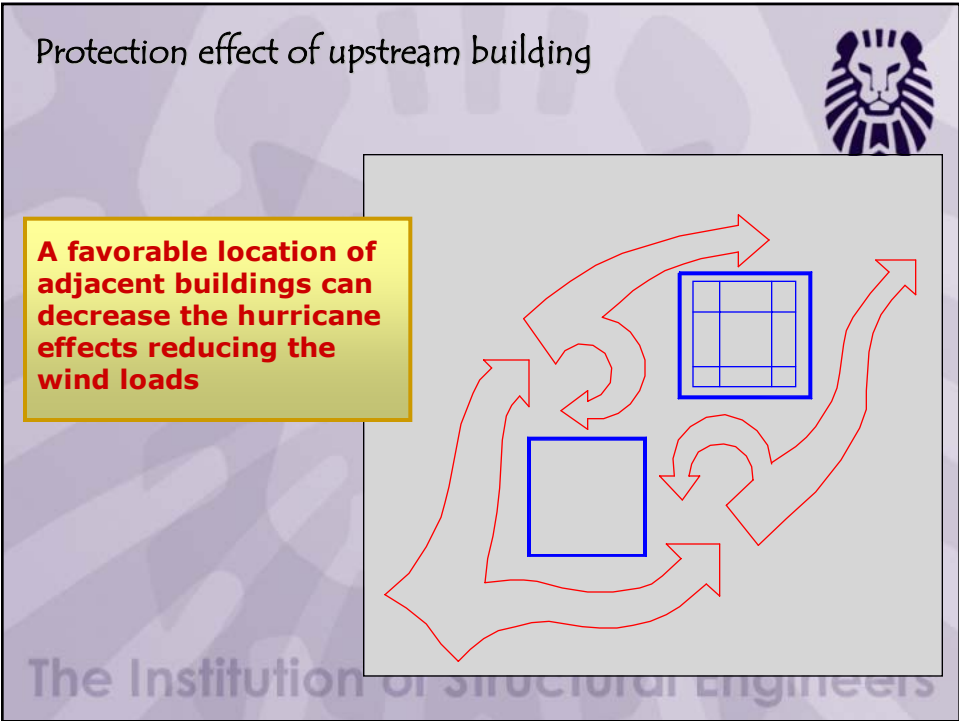
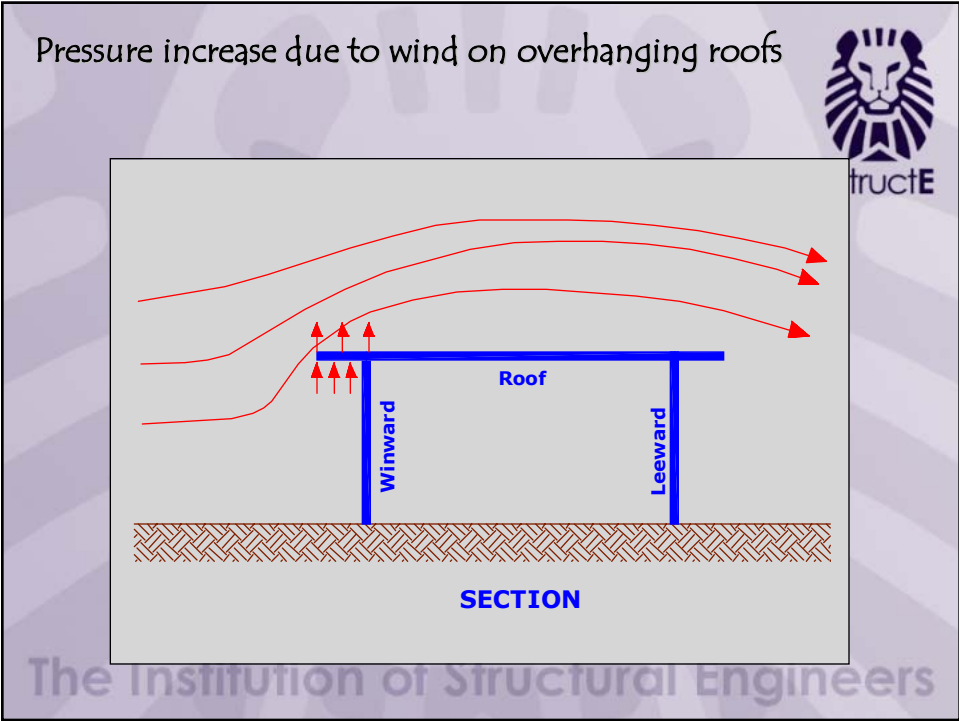
Turbulent flow on high rise buildings due to upwind obstructions



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Unfavorable location of an adjacent building

A bad location of nearby buildings might induce increase of wind loads

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Pressure coefficients on high rise buildings

Pressure coefficients on high rise buildings

Pressure varies with height (Windward)

Pressure keeps constant with height (Leeward)

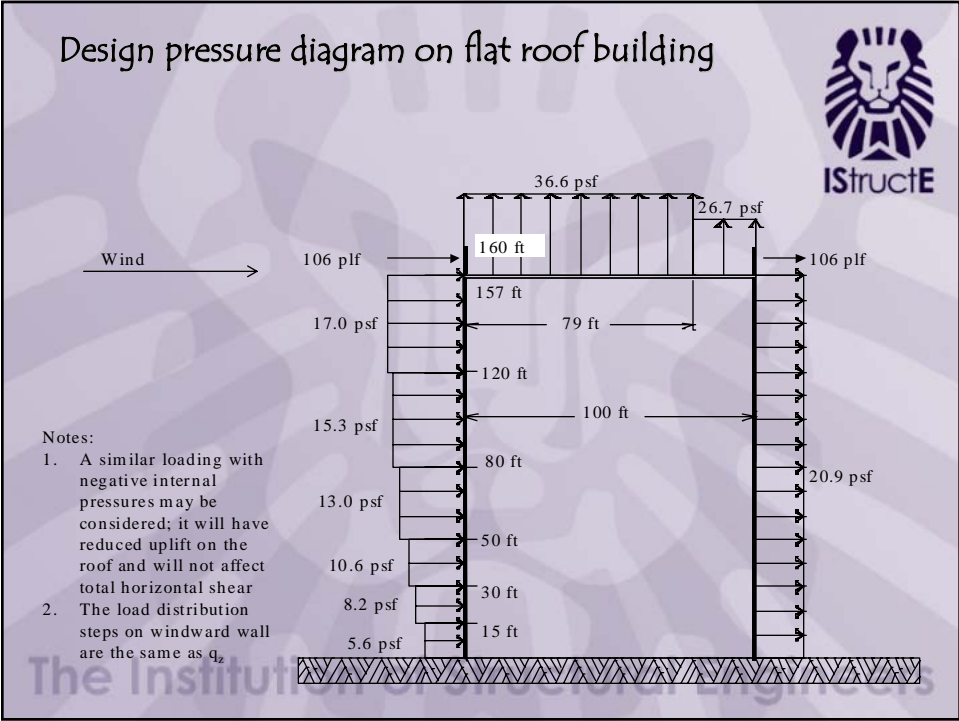
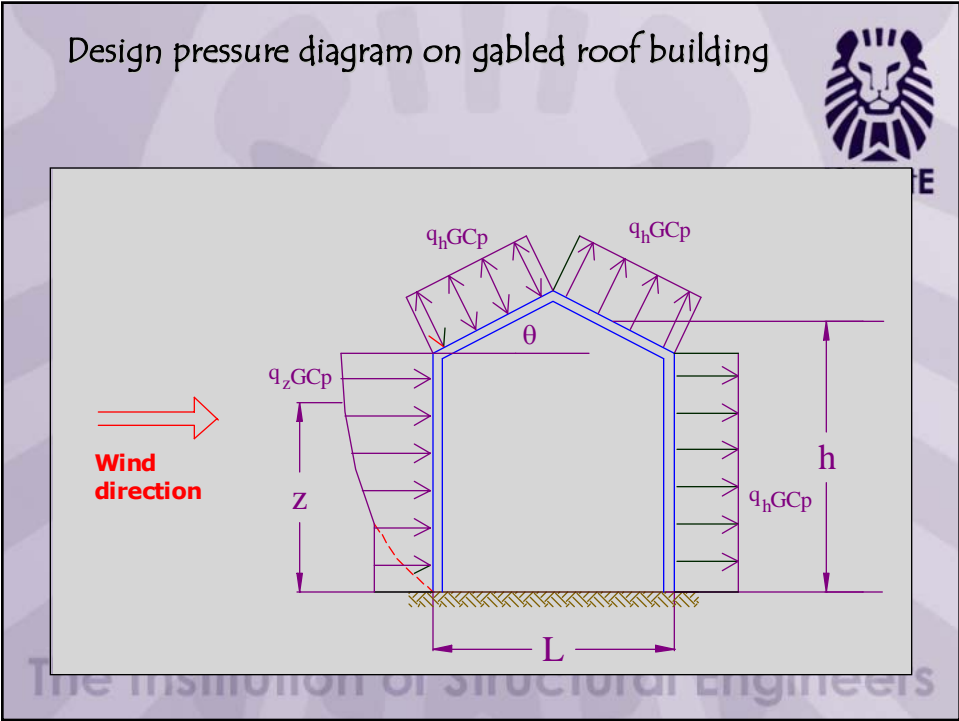
ROOF -0.6

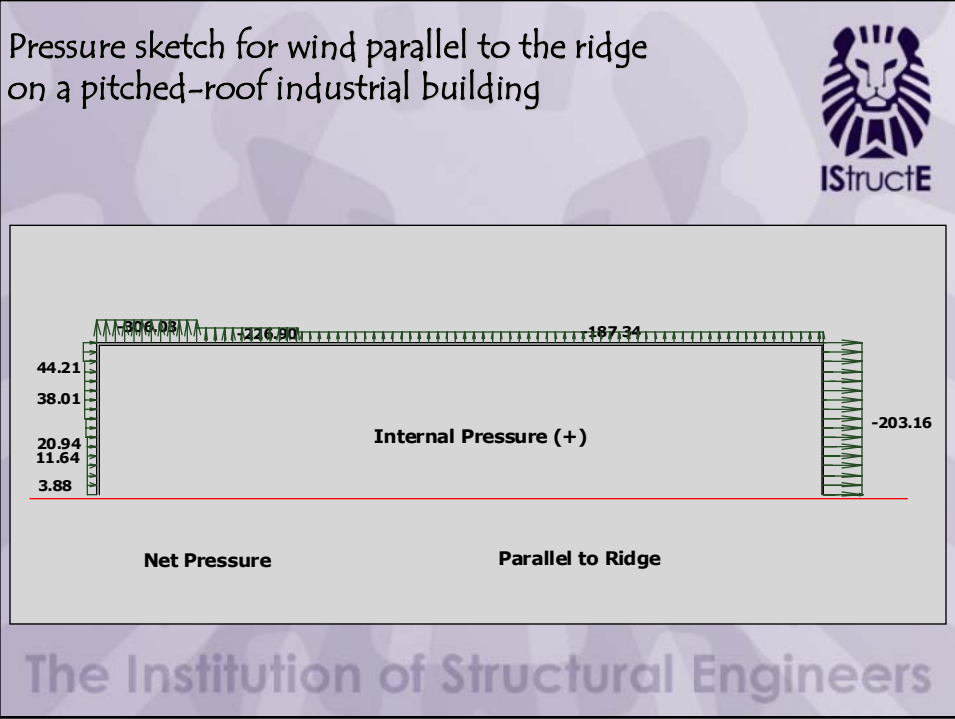
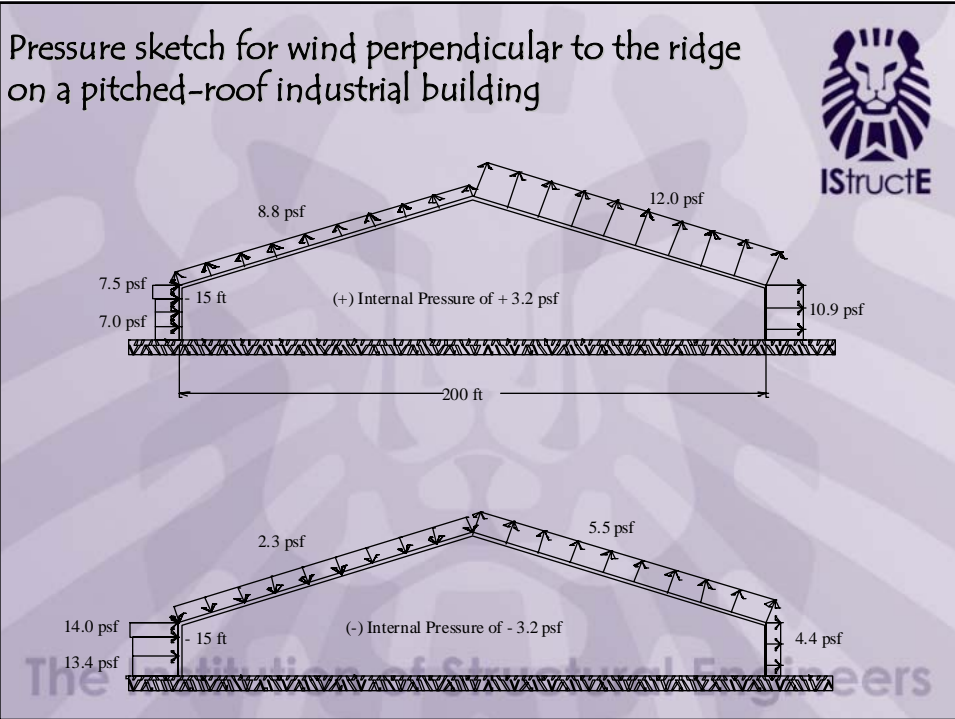
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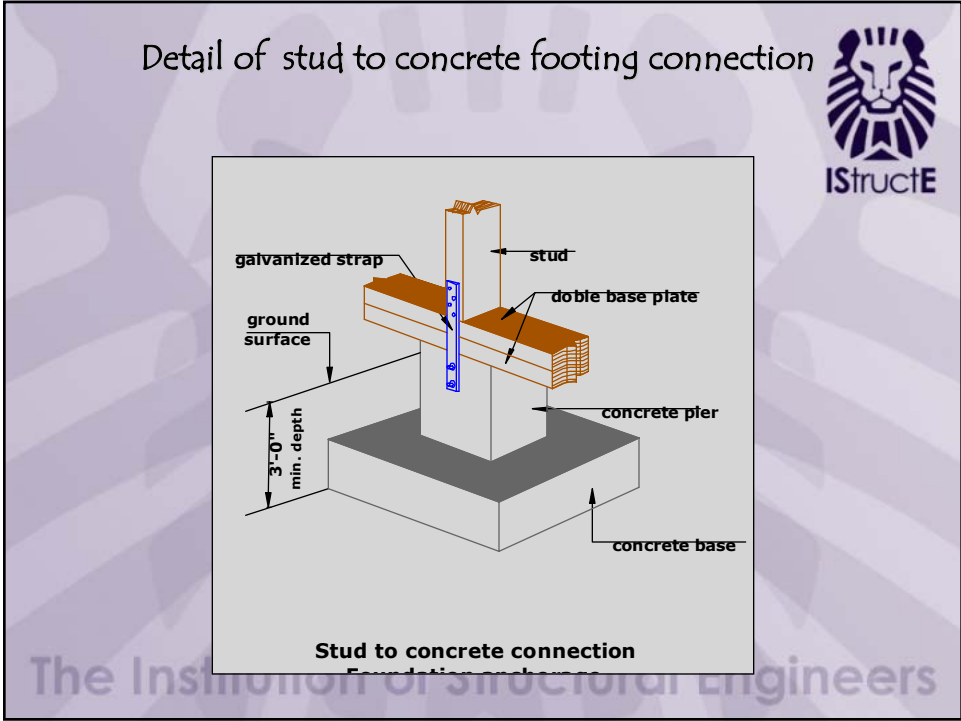
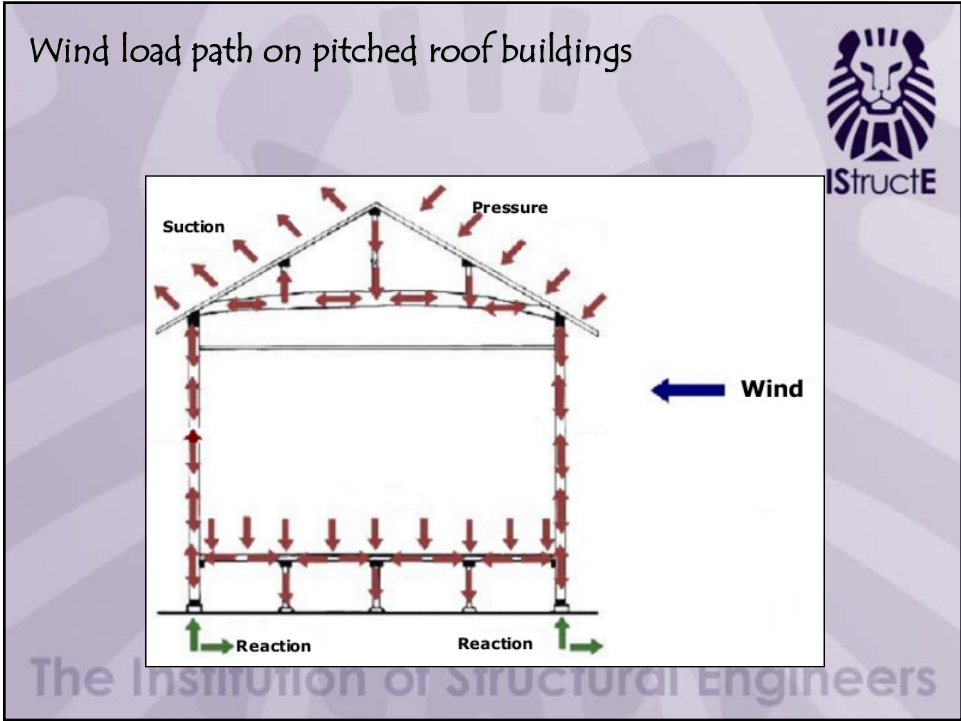
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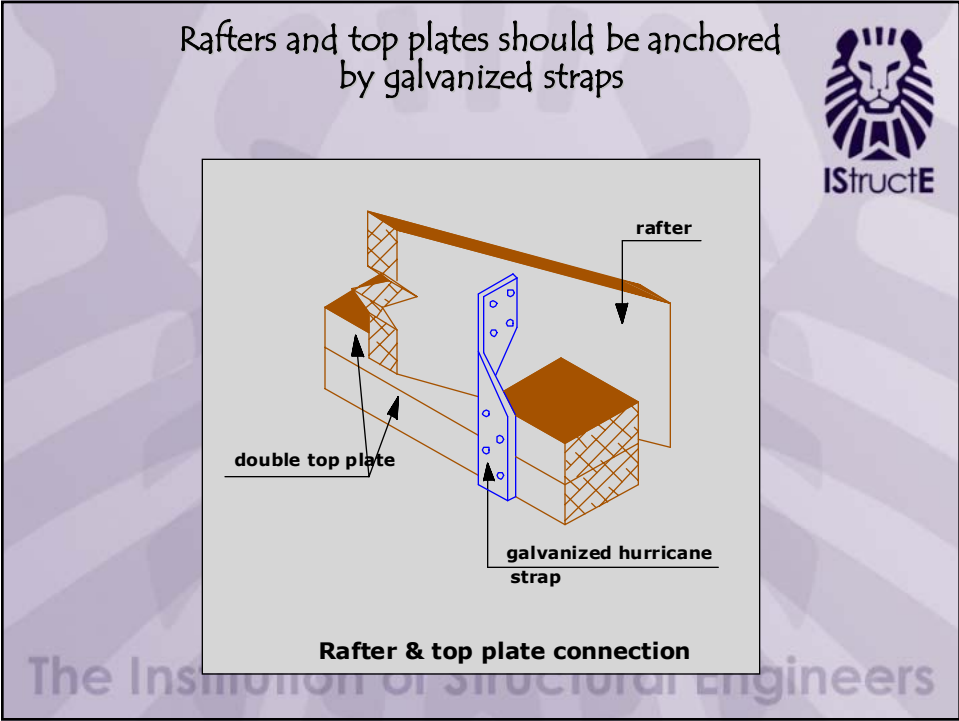
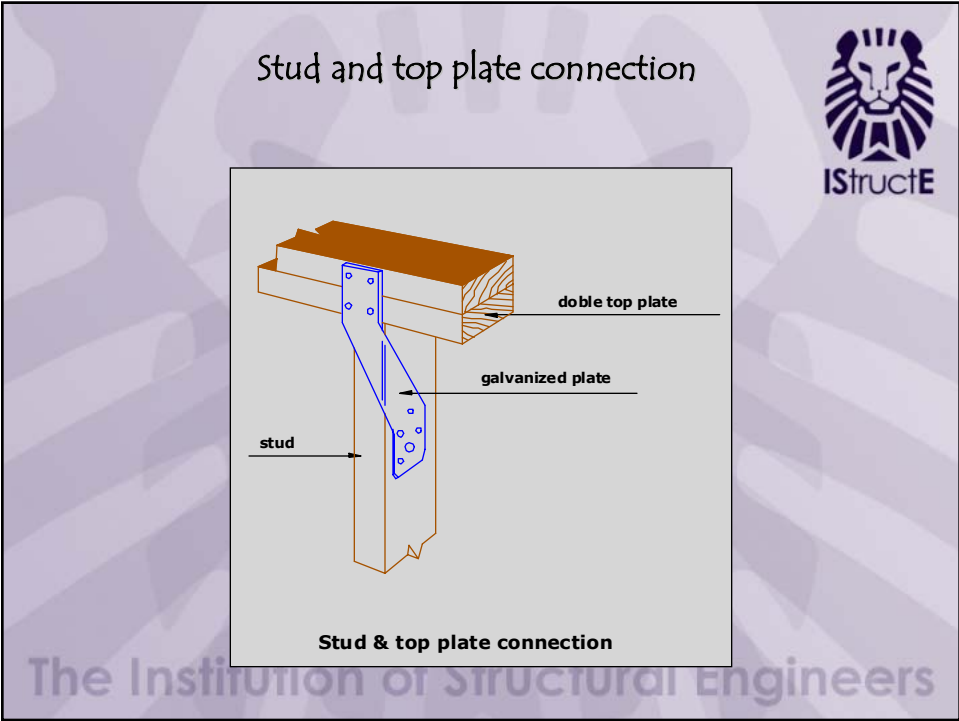
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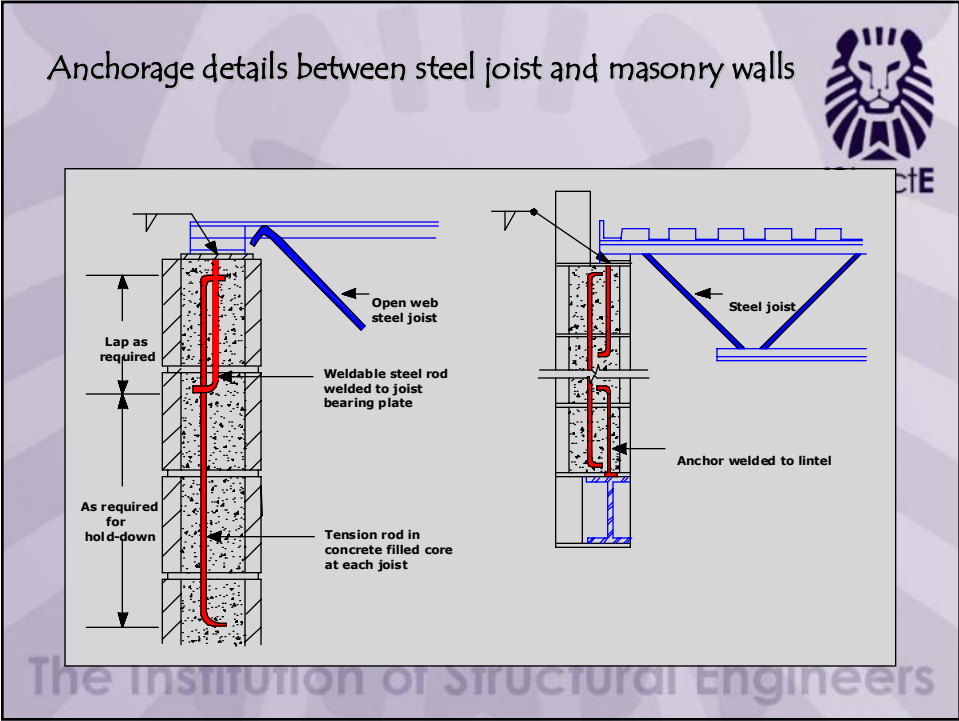
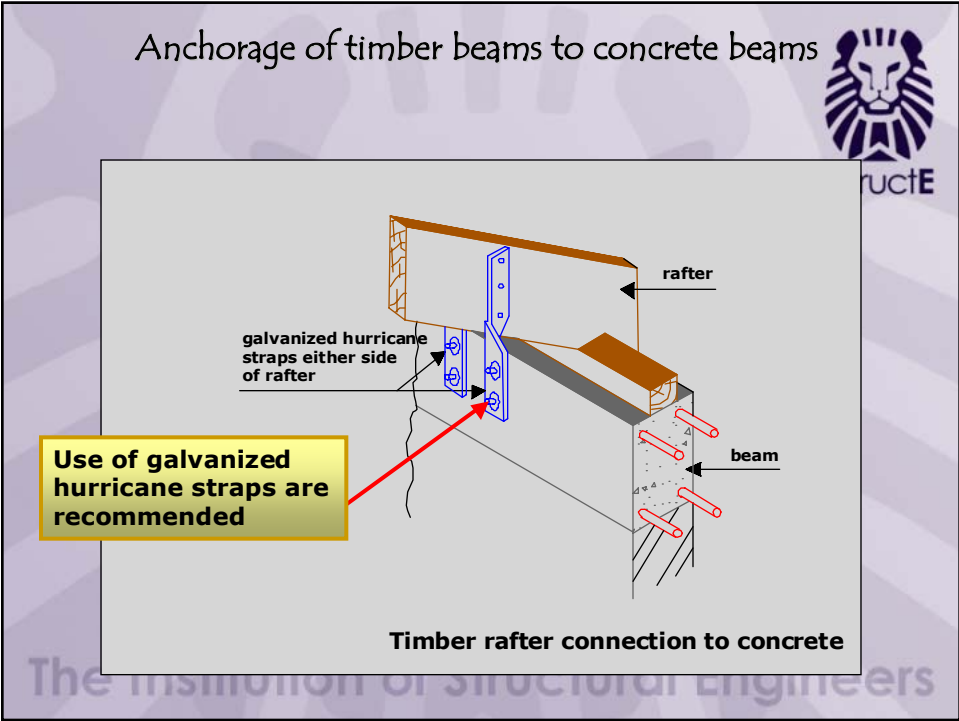
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Hipped roof recommended over flat roof

Hatched area indicates where more frequent fixings are required

PLAN ISOMETRIC

Hipped roof

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The diagram illustrates a hipped roof design. On the left, a 'PLAN' view shows a rectangular footprint with four sloping sides meeting at a central point. The roof surface is indicated by a hatched pattern. On the right, an 'ISOMETRIC' view shows a 3D perspective of a house with a hipped roof. The roof's surface is also hatched. A text label 'Hatched area indicates where more frequent fixings are required' has arrows pointing to the hatched areas in both views. The Institution of Structural Engineers logo is in the top right corner.

Gabled roof with slopes of 20 to 30 degrees are preferred against hurricanes

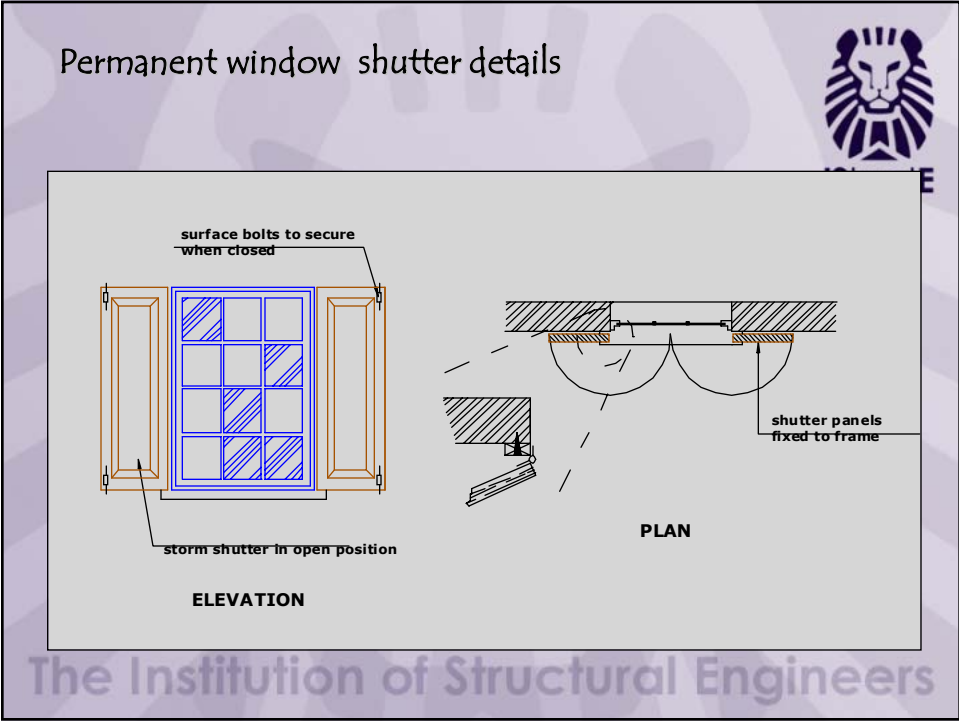
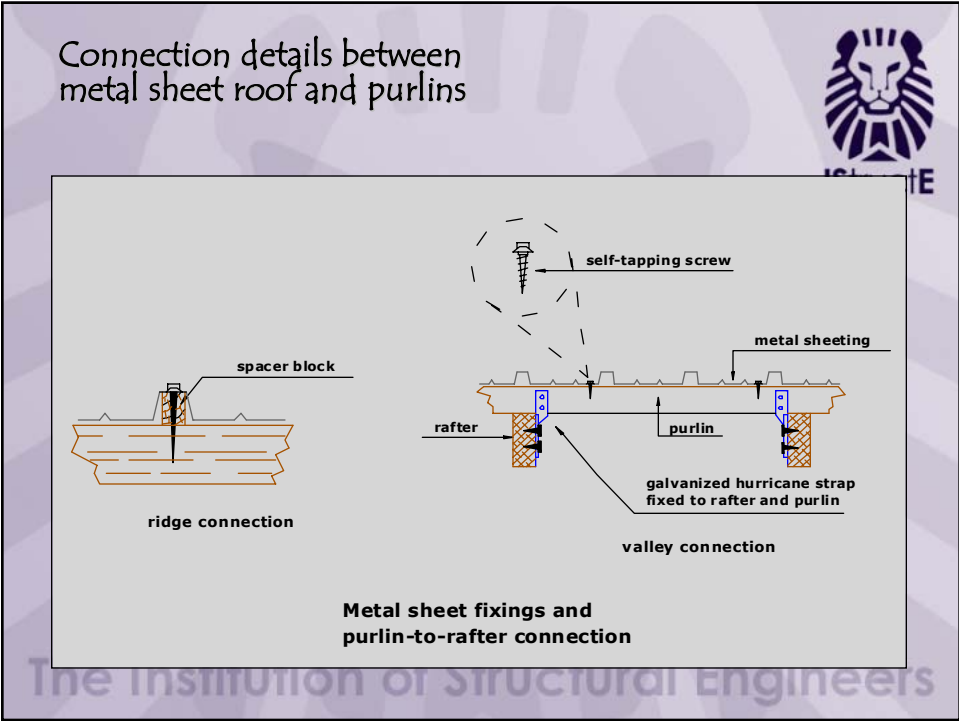
hatched area indicates where more frequent fixings are required

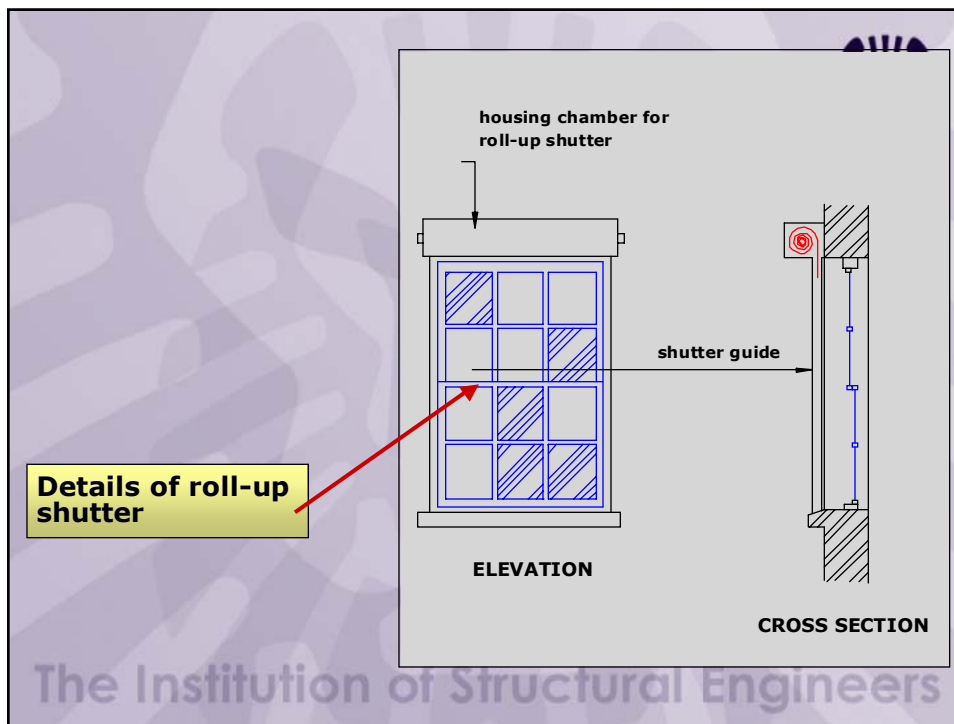
PLAN ISOMETRIC

gabled roof

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The diagram illustrates a gabled roof design. On the left, a 'PLAN' view shows a rectangular footprint with two sloping sides meeting at a central ridge. The roof surface is indicated by a hatched pattern. On the right, an 'ISOMETRIC' view shows a 3D perspective of a house with a gabled roof. The roof's surface is also hatched. A text label 'hatched area indicates where more frequent fixings are required' has arrows pointing to the hatched areas in both views. The Institution of Structural Engineers logo is in the top right corner.





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Summary for Method 2



- MWFRS

$$p = q GC_p - q_i (GC_{pi})$$

- C&C for $h \leq 60$ ft

$$p = q_h [(GC_p) - (GC_{pi})]$$

- where:

$$q_z = 0.00256 K_z K_{zt} K_d V^2 I$$

$$q_h = 0.00256 K_h K_{zt} K_d V^2 I$$

p = design pressure
q = effective velocity pressure
G = gust effect factor (gef)
C_p = external pressure coefficient
q_i = velocity pressure (internal)
GC_{pi} = gef + internal pressure coefficient
GC_p = gef + external pressure coefficient

K_z = exposure velocity pressure coefficient
K_{zt} = topographic factor
K_d = directionality factor
V = basic wind speed
I = importance factor

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